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Fehr \& Peers

TRANSPORTATION CONSULTANTS

July 15, 2011

Ms. Polly Chapman
P.O. Box 2490

31301 Highway 3
Weaverville, CA 96093

## Re: Traffic Signalization Study

Dear Ms. Chapman:
This letter report provides traffic operations analysis results for the SR 299 (Main Street) corridor through Weaverville, California. The following timeframes were studied:

- Existing Conditions
- 2009 Conditions (with East Connector)
- 2040 Conditions (with East Connector)

Existing intersection turning movement counts were collected in July 2009. Intersection turning movement volumes were developed for 2009 and 2040 conditions (with East Connector), using the Trinity County travel demand model.

The purpose of this study is to develop intersection improvements on SR 299 in Weaverville that work efficiently as a system. A summary of the analysis results is provided in the tables on pages 14, 15, and 16. A summary of the findings and recommendations is provided on page 16.

This analysis also looks at the effects of converting Center Street between Court Street and SR 3 from a one-way section to a two-way section.

## STUDY INTERSECTIONS AND ANALYSIS SCENARIOS

The following study intersections along the SR 299 (Main Street) corridor were analyzed:

1. SR 299/Glen Road-East Connector
2. SR 299/Washington Street
3. SR 299/SR 3 (Trinity Lake Boulevard)
4. SR 299/Garden Gulch Street-Forest Avenue

Intersection level of service, vehicle queuing, travel time, and greenhouse gas emissions analyses were performed for the SR 299 corridor assuming three scenarios.

- Unsignalized Intersections - The study intersections were analyzed under existing conditions based on intersection turning movement counts collected in July 2009.
- Signalized Intersections - The SR 299 corridor was analyzed assuming the four study intersections are signalized under 2009 conditions (with East Connector) and 2040 conditions (with East Connector).
- Signalized and Roundabout Intersections - The SR 299 corridor was analyzed assuming the SR 299/Glen Road-East Connector and SR 299/Garden Gulch Street-Forest Avenue intersections are roundabouts, and the SR 299/Washington Street and SR 299/SR 3 intersections are signalized. 2009 conditions (with East Connector) and 2040 conditions (with East Connector) were analyzed.

The SR 299/Glen Road-East Connector intersection was also analyzed as an unsignalized (side street stop controlled) intersection under 2009 conditions (with East Connector) and 2040 conditions (with East Connector) and compared to the Trinity County level of service thresholds.

## ANALYSIS METHODOLOGY

## Signal Warrants

The Federal Highway Administration's (FHWA) Manual on Uniform Traffic Control Devices (MUTCD) provides Four Hour and Peak Hour signal warrants, which are commonly used to determine if an intersection is in need of a traffic signal.

According to the MUTCD, the Four Hour signal warrant conditions are intended to be applied where the volume of intersecting traffic is the principal reason to consider installing a traffic control signal. The Four Hour warrant compares the traffic volumes from any four hours of an average day on the major street (total of both directions) to the corresponding vehicle volume on the higher-volume minor street approach (one direction only).

The Peak Hour signal warrant is intended for use at a location where traffic conditions are such that for a minimum of one hour of an average day, the minor street traffic suffers undue delay when entering or crossing the major street. (MUTCD) The Peak Hour warrant compares the traffic volumes for one hour of an average day on the major street (total of both directions) to the corresponding vehicle volume on the higher-volume minor street approach (one direction only).

The MUTCD provides separate signal warrants for urban and rural areas. For communities with a population of less than 10,000, the rural area signal warrant criteria should be applied. The Weaverville population is less than 10,000 , therefore the rural area criteria was applied.

## Intersection Analysis

Transportation engineers and planners commonly use the term level of service (LOS) to measure and describe the operational status of the local roadway network. An intersection or roadway segment's level of service can range from LOS A (indicating free-flow traffic conditions with little or no delay), to LOS F (representing oversaturated conditions where traffic flows exceed design capacity, resulting in long queues and delays).

## Signalized Intersections

The level of service at signalized intersections was determined using the methodology contained in Chapter 16 of the Highway Capacity Manual (HCM) 2000. The HCM 2000 methodology
determines the level of service at signalized intersections by comparing the average control delay for all vehicles approaching the intersection to the delay thresholds shown in Table 1.

## Unsignalized Intersections

Unsignalized (side-street stop controlled) intersection level of service analysis was performed using the methodology in Chapter 17 of HCM 2000. The HCM 2000 methodology determines the level of service at unsignalized intersections by comparing the average control delay for each individual movement to the delay thresholds shown in Table 1.

TABLE 1
INTERSECTION LEVEL OFSERVICE DEFINITIONS

| Level of <br> Service | Description | Signalized <br> Intersections <br> (Average Control <br> Delay) $^{\mathbf{1}}$ | Unsignalized <br> Intersections <br> (Average Control <br> Delay) ${ }^{2}$ |
| :---: | :---: | :---: | :---: |
| A | Represents free flow. Individual users are virtually <br> unaffected by others in the traffic stream. | $\leq 10$ | $\leq 10$ |
| B | Stable flow, but the presence of other users in the <br> traffic stream begins to be noticeable. | $>10$ to 20 | $>10$ to 15 |
| C | Stable flow, but the operation of individual users <br> becomes significantly affected by interactions with <br> others in the traffic stream. | $>20$ to 35 | $>15$ to 25 |
| D | Represents high-density, but stable flow. | $>35$ to 55 | $>25$ to 35 |
| E | Represents operating conditions at or near the |  |  |
| capacity level. | $>55$ to 80 | $>35$ to 50 |  |
| F | Represents forced or breakdown flow. | $>80$ | $>50$ |
| Seres |  |  |  |

Sources:
${ }^{1}$ HCM 2000, Chapter 16, Signalized Intersections. Values shown are in seconds/vehicle.
${ }^{2}$ HCM 2000, Chapter 17, Unsignalized Intersections. Values shown are in seconds/vehicle.

## Level of Service Thresholds

The Trinity County Regional Transportation Plan (RTP) (2010) identifies level of service thresholds for roadways and intersections within the county. The RTP states:

The minimum acceptable Level of Service (LOS) standard for county roadway and intersection operation in the Weaverville Community Plan Area is " $D$ ". For unsignalized intersections, LOS is calculated based upon the average peak hour delay for the worst approach (using the current version of the Highway Capacity Manual). No public highway or roadway within the Weaverville Community Plan Area should be allowed to fall to or below LOS "E".

## CORRIDOR ANALYSIS

## Signal Warrant Analysis

The Four Hour and Peak Hour signal warrants were analyzed for each of the study intersections based on the existing intersection turning movement volumes (from counts collected in July 2009) and the 2040 model volumes (with East Connector). Table 2 shows the results of the signal warrant analysis. The technical analysis is provided in the Attachment A.

| TABLE 2 <br> SIGNAL WARRANT ANALYSIS RESULTS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection | Warrant Met? (Yes/No) |  |  |  |
|  | Existing Conditions |  | 2040 Conditions (with East Connector) |  |
|  | Four Hour Warrant | Peak Hour Warrant | Four Hour Warrant | Peak Hour Warrant |
| SR 299/Glen Road-East Connector | Yes* | Yes* | Yes | Yes |
| SR 299/Washington Street | Yes | No | Yes | Yes |
| SR 299/SR 3 | No | No | Yes | Yes |
| SR 299/Garden Gulch Street | No | No | No | No |

Notes: * Based on 2009 Conditions (with East Connector) traffic volumes.
Source: Fehr \& Peers, 2011

As shown in Table 2, the SR 299/Glen Road-East Connector intersection passes the Four Hour and Peak Hour signal warrants under 2009 conditions (with East Connector) and 2040 conditions (with East Connector). The SR 299/Washington Street intersection passes the Four Hour signal warrant, but not the Peak Hour signal warrant under existing conditions (based on the existing intersection turning movement counts). The SR 299/SR 3 intersection meets the Four Hour and Peak Hour signal warrants under 2040 conditions (with East Connector). The SR 299/Garden Gulch intersection does not meet traffic signal warrant criteria under any condition.

## Scenario 1: Unsignalized Intersections

Scenario 1 analyzes the SR 299 corridor with side street stop controls at the study intersections. Existing conditions, 2009 conditions (with East Connector), and 2040 conditions (with East Connector) traffic volumes were analyzed under this scenario.

## Level of Service

Level of service analysis was performed at the study intersections using Synchro Version 6.0 software. The existing conditions analysis is based on intersection turning movement volumes collected in July 2009. The 2009 conditions (with East Connector) and 2040 conditions (with East Connector) traffic volumes were determined using the travel demand model. Table 3 shows the level of service results with unsignalized study intersections. The technical analysis is provided in the Attachment B.

TABLE 3
LEVEL OF SERVICE RESULTS (UNSIGNALIZED INTERSECTIONS)

| Intersection | Control Type ${ }^{1}$ | PM Peak |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Existing Conditions |  | 2009 Conditions (with East Connector) |  | 2040 Conditions (with East Connector) |  |
|  |  | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS |
| SR 299/Glen Road | SSSC | 24.7 | C | -- | -- | -- | -- |
| SR 299/Glen Road-East Connector | SSSC | -- | -- | 42.8 | E | 80.3 | F |
| SR 299/Washington Street | SSSC | 44.0 | E | 27.8 | D | 128.1 | F |
| SR 299/SR 3 | SSSC | 16.7 | C | 17.2 | C | 15.7 | C |
| SR 299/Garden Gulch Street | SSSC | 20.9 | C | 22.9 | C | 29.7 | D |

Notes: ${ }^{1}$ SSSC = Side Street Stop Control
${ }^{2}$ Delay is reported in seconds per vehicle for the worst movement for unsignalized intersections.
Source: Fehr \& Peers, 2011
The side street approach of the SR 299/Washington Street intersection operates at an unacceptable level of service under existing conditions. When the East Connector is constructed, a significant amount of existing traffic will shift from Washington Street to the East Connector, improving the level of service at the SR 299/Washington Street intersection to LOS D, but diminishing the level of service at the SR 299/Glen Road-East Connector intersection to LOS E under 2009 conditions. The analysis indicates that if the East Connector is constructed without a traffic signal at SR 299, the intersection will not meet the Trinity County LOS standard.

Under 2040 conditions, two of the four study intersections will operate at unacceptable levels of service with unsignalized intersections.

## Travel Time Through Corridor

The time it takes a vehicle to travel from one end of the SR 299 corridor to the other was analyzed using SimTraffic micro-simulation software. For the purposes of this analysis the corridor is defined as the section between the SR 299/Martin Street intersection and the SR 299/ Garden Gulch Street-Forest Avenue intersection. The total corridor length is approximately 1.25 miles. Table 4 shows the travel time results for the corridor with unsignalized study intersections.

TABLE 4
TRAVEL TIME THROUGH SR 299 CORRIDOR (WITH UNSIGNALIZED INTERSECTIONS)

| Direction of Travel | Travel Time |  |  |
| :---: | :---: | :---: | :---: |
|  | Existing Conditions | $\mathbf{2 0 0 9}$ Conditions <br> (with East Connector) | $\mathbf{2 0 4 0}$ Conditions <br> (with East Connector) |
| Northbound | 2.9 minutes | 3.1 minutes | 3.1 minutes |
| Southbound | 3.4 minutes | 3.4 minutes | 3.4 minutes |

Notes: The analysis includes the section of SR 299 between the SR 299/Martin Street and SR 299/Garden Gulch Street-Forest Avenue intersections.
Source: Fehr \& Peers, 2011

The total travel time through the corridor with unsignalized intersections ranges from approximately 3 to $31 / 2$ minutes for the three study timeframes.

## Greenhouse Gas Emissions

Greenhouse gas emissions were analyzed using Synchro software. Carbon monoxide, nitrogen oxides, and volatile organic compound emissions were analyzed at the study intersections. The emissions results are shown in Table 5. The technical analysis is provided in the Attachment $\mathbf{B}$.

| TABLE 5 <br> GREENHOUSE GAS EMISSIONS RESULTS (WITH UNSIGNALIZED INTERSECTIONS) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Emissions ${ }^{1}$ |  |  |  |  |  |
|  | Existing Conditions |  |  | 2040 Conditions (with East Connector) |  |  |
|  | CO | $\mathrm{NO}_{\mathrm{X}}$ | VOC | CO | $\mathrm{NO}_{\mathrm{X}}$ | VOC |
| SR 299/Glen Road-East Connector | 1.02 | 0.20 | 0.24 | 1.13 | 0.22 | 0.26 |
| SR 299/Washington Street | 1.40 | 0.27 | 0.33 | 0.74 | 0.14 | 0.17 |
| SR 299/SR 3 | 0.80 | 0.16 | 0.19 | 0.50 | 0.10 | 0.12 |
| SR 299/Garden Gulch Street | 0.52 | 0.10 | 0.12 | 0.58 | 0.11 | 0.13 |
| Notes: ${ }^{1} \mathrm{CO}=$ Carbon Monoxide, $\mathrm{NO}_{\mathrm{x}}=$ Nitrogen Oxides, $\mathrm{VOC}=$ Volatile Organic Compounds Emissions reported in kilograms (for the peak hour). <br> Source: Fehr \& Peers, 2011 |  |  |  |  |  |  |

## Scenario 2: Signalized Intersections

Scenario 2 analyzes the SR 299 corridor assuming the study intersections are signalized. 2009 conditions (with East Connector) and 2040 conditions (with East Connector) traffic volumes were analyzed under this scenario.

## Level of Service

Intersection level of service was analyzed during the summer PM peak period for 2009 conditions (with East Connector) and 2040 conditions (with East Connector) using Synchro software. Table 6 shows the level of service results assuming the study intersections are signalized. The technical analysis is provided in the Attachment C.

| TABLE 6 <br> LEVEL OF SERVICE RESULTS (WITH SIGNALS) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Control Type | 2009 Conditions (with East Connector) |  | 2040 Conditions (with East Connector) |  |
|  |  | PM Peak |  | PM Peak |  |
|  |  | Delay ${ }^{1}$ | LOS | Delay ${ }^{1}$ | LOS |
| SR 299/Glen Road-East Connector | Signal | 13.7 | B | 13.9 | B |
| SR 299/Washington Street | Signal | 10.3 | B | 11.9 | B |
| SR 299/SR 3 | Signal | 10.4 | B | 11.6 | B |
| SR 299/Garden Gulch Street | Signal | 11.8 | B | 15.3 | B |

Notes: ${ }^{1}$ Delay is reported in seconds per vehicle for the overall intersection for signalized intersections.
Source: Fehr \& Peers, 2011
As shown in the table, the study intersections operate at LOS B with traffic signals under 2009 and 2040 conditions (with East Connector).

## Vehicle Queuing

Vehicle queuing along the SR 299 corridor was analyzed using SimTraffic micro-simulation software. Table 7 shows the vehicle queuing results at the study intersections. The average and maximum queues are shown for each approach of the intersection. The technical analysis is provided in the Attachment C.

TABLE 7
VEHICLE QUEUING RESULTS (WITH SIGNALS)

| Intersection | Intersection Approach | Distance to Closest Intersection (feet) ${ }^{1}$ | 2009 Conditions (with East Connector) |  | 2040 Conditions (with East Connector) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | PM Peak Queue Lengths |  | PM Peak Queue Lengths |  |
|  |  |  | Average feet (cars ${ }^{2}$ ) | Maximum feet (cars ${ }^{2}$ ) | Average feet (cars ${ }^{2}$ ) | Maximum feet (cars ${ }^{2}$ ) |
| SR 299/Glen RoadEast Connector | NB | 960 | 70 (3) | 170 (7) | 90 (4) | 230 (10) |
|  | SB | 460 | 60 (3) | 180 (8) | 75 (3) | 205 (9) |
|  | EB | $230^{3}$ | 50 (2) | 115 (5) | 60 (3) | 130 (6) |
|  | WB | N/A | 35 (2) | 85 (4) | 40 (2) | 95 (4) |
| SR 299/Washington Street | NB | 540 | 55 (3) | 180 (8) | 90 (4) | 290 (12) |
|  | SB | 355 | 65 (3) | 170 (7) | 90 (4) | 255 (11) |
|  | EB | 690 | 30 (2) | 65 (3) | 30 (2) | 70 (3) |
|  | WB | 775 | 25 (1) | 75 (3) | 50 (2) | 120 (5) |
| SR 299/SR 3 | NB | 225 | 70 (3) | 200 (8) | 75 (3) | 210 (9) |
|  | SB | 530 | 40 (2) | 95 (4) | 50 (2) | 140 (6) |
|  | WB | 280 | 35 (2) | 80 (4) | 40 (2) | 95 (4) |
| SR 299/Garden Gulch Street | NB | 230 | 35 (2) | 125 (5) | 40 (2) | 140 (6) |
|  | SB | 175 | 50 (2) | 150 (6) | 65 (3) | 170 (7) |
|  | EB | 295 | 20 (1) | 55 (3) | 25 (1) | 60 (3) |
|  | WB | 1230 | 30 (2) | 75 (3) | 35 (2) | 80 (4) |

Notes: ${ }^{1}$ Distance estimated using Google Maps.
${ }^{2}$ The vehicle queue length was calculated assuming an average car length of 25 feet. A queue length of 5-25 feet is considered one vehicle, $26-50$ feet is two vehicles, etc. The queuing results are also a product of a simulation that is designed to represent "real-life" drivers to the best extent possible. Therefore, each simulation run represents a unique set of data. An average of 10 runs is shown in the results table.
${ }^{3}$ This is the distance to Fairway Drive. Nugget Lane is marked "Keep Clear" and was therefore excluded. Analysis performed assuming the SR 299 corridor is the North-South direction.
Source: Fehr \& Peers, 2011
The vehicle queues are not expected to spill back into adjacent intersections. Vehicle queues at the study intersections are only expected during the peak traffic periods and dissipate quickly.

## Travel Time Through Corridor

Travel time through the SR 299 corridor was analyzed for 2009 conditions and 2040 conditions assuming construction of the East Connector road is complete and the study intersections are signalized. The results are shown in Table 8. The technical analysis is in the Attachment C.

TABLE 8
TRAVEL TIME THROUGH SR 299 CORRIDOR (WITH SIGNALS)

| Direction of Travel | Travel Time |  |
| :---: | :---: | :---: |
|  | $\mathbf{2 0 0 9}$ Conditions <br> (with East Connector) | $\mathbf{2 0 4 0}$ Conditions <br> (with East Connector) |
| Northbound | 4.2 minutes | 4.3 minutes |
| Southbound | 3.8 minutes | 3.9 minutes |

Notes: The analysis includes the section of SR 299 between the SR 299/Martin Street and SR 299/Garden Gulch StreetForest Avenue intersections.
Source: Fehr \& Peers, 2011
The total travel time through the corridor, with traffic signals at the study intersections, is approximately 4 minutes, which is an increase of $1 / 2-1 \frac{1}{2}$ minute over the existing travel time.

## Greenhouse Gas Emissions

Greenhouse gas emissions were analyzed using Synchro software. Carbon monoxide, nitrogen oxides, and volatile organic compound emissions were analyzed at the study intersections. The emissions results are shown in Table 9. The technical analysis is provided in the Attachment C.

| TABLE 9GREENHOUSE GAS EMISSIONS RESULTS (WITH SIGNALS) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Emissions ${ }^{1}$ |  |  |  |  |  |
|  | 2009 Conditions (with East Connector) |  |  | 2040 Conditions (with East Connector) |  |  |
|  | CO | $\mathrm{NO}_{\mathrm{x}}$ | VOC | CO | $\mathrm{NO}_{\mathrm{x}}$ | VOC |
| SR 299/Glen Road-East Connector | 1.01 | 0.20 | 0.23 | 1.14 | 0.22 | 0.27 |
| SR 299/Washington Street | 0.56 | 0.11 | 0.13 | 0.88 | 0.17 | 0.20 |
| SR 299/SR 3 | 0.50 | 0.10 | 0.12 | 0.65 | 0.13 | 0.15 |
| SR 299/Garden Gulch Street | 0.58 | 0.11 | 0.13 | 0.70 | 0.14 | 0.16 |
| Notes: ${ }^{1} \mathrm{CO}=$ Carbon Monoxide, $\mathrm{NO}_{\mathrm{x}}=$ Nitrogen Oxides, $\mathrm{VOC}=$ Volatile Organic Compounds Emissions reported in kilograms (for the peak hour). <br> Source: Fehr \& Peers, 2011 |  |  |  |  |  |  |

The 2009 conditions (with East Connector) greenhouse gas emissions increase at some intersections and decrease at some intersections compared to existing conditions analysis results because the traffic volumes at the intersections change due to the East Connector. Therefore, the existing conditions and 2009 conditions (with East Connector) analysis results cannot be compared directly because the scenarios do not share a common baseline.

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The 2040 conditions (with East Connector) with signalized intersections emissions results increase at all of the study intersections compared to the 2040 conditions with unsignalized intersections emissions results. The traffic volumes at the study intersections were the same for both scenarios. The traffic signals increased the emissions at the study intersections by small amounts (less than 0.20 kilograms). The emissions increase at the study intersections under the signals scenario due to additional stopping and accelerating of through traffic on SR 299. Without a traffic signal, the through movements on SR 299 are freely flowing and do not have to stop and start at intersections.

## Vibration Analysis

A Traffic Vibration Assessment was performed by Bollard Acoustical Consultants, Inc. to determine if installing traffic signals at the study intersections would increase noise and roadway vibration caused by heavy trucks. The concern is that heavy trucks will have to stop along SR 299, where there are currently no controls, increasing vibration and noise to an unacceptable level. The analysis shows that traffic signals at the study intersections will not cause a significant increase in vibration along the SR 299 corridor. The Trinity County Intersection Improvement Traffic Vibration Assessment report (Bollard Acoustical Consultants, Inc.) is provided in Attachment E .

## Scenario 3: Signalized and Roundabout Intersections

Scenario 3 analyzes the SR 299 corridor assuming:

- Traffic signals at:
o SR 299/Washington Street
o SR 299/SR 3
- Roundabouts at:
o SR 299/Glen Road-East Connector
o SR 299/Garden Gulch Street
2009 conditions (with East Connector) and 2040 conditions (with East Connector) traffic volumes were analyzed under this scenario.


## Level of Service

Table 10 shows the level of service results at the study intersections assuming traffic signals and roundabouts at the study intersections. The technical analysis is provided in Attachment $\mathbf{D}$.

## TABLE 10

LEVEL OF SERVICE RESULTS (WITH SIGNALS AND ROUNDABOUTS)

| Intersection | Control Type | 2009 Conditions (with East Connector) |  | 2040 Conditions (with East Connector) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PM Peak |  | PM Peak |  |
|  |  | Delay ${ }^{1}$ | LOS | Delay ${ }^{1}$ | LOS |
| SR 299/Glen Road-East Connector | Roundabout | 9.1 | A | 9.5 | A |
| SR 299/Washington Street | Signal | 10.3 | B | 11.9 | B |
| SR 299/SR 3 | Signal | 10.4 | B | 11.6 | B |
| SR 299/Garden Gulch Street | Roundabout | 7.6 | A | 7.9 | A |

Notes: ${ }^{1}$ Delay is reported in seconds per vehicle for the overall intersection for signalized and roundabout intersections. Source: Fehr \& Peers, 2011

As shown in the table, the study intersections operate at LOS B or better with roundabouts and traffic signals under 2009 and 2040 conditions (with East Connector).

## Vehicle Queuing

Table 11 shows the vehicle queuing results at the study intersections. The average and maximum queues are shown for each approach of the intersection. The technical analysis is provided in the Attachment D.

TABLE 11
VEHICLE QUEUING RESULTS (WITH SIGNALS AND ROUNDABOUTS)

| Intersection | Intersection Approach | Distance to Closest Upstream Intersection (feet) ${ }^{1}$ | 2009 Conditions (with East Connector) |  | 2040 Conditions (with East Connector) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | PM Peak Queue Lengths |  | PM Peak Queue Lengths |  |
|  |  |  | Average feet (cars ${ }^{2}$ ) | Maximum feet ( cars $^{2}$ ) | Average feet (cars ${ }^{2}$ ) | Maximum feet (cars ${ }^{2}$ ) |
| SR 299/Glen RoadEast Connector | NB | 960 | 50 (2) | 120 (5) | 60 (3) | 145 (6) |
|  | SB | 460 | 45 (2) | 130 (6) | 50 (2) | 135 (6) |
|  | EB | $230^{3}$ | 35 (2) | 75 (3) | 35 (2) | 80 (4) |
|  | WB | N/A | 25 (1) | 60 (3) | 30 (2) | 75 (3) |
| SR 299/Washington Street | NB | 540 | 55 (3) | 160 (7) | 80 (4) | 250 (10) |
|  | SB | 355 | 60 (3) | 170 (7) | 90 (4) | 220 (9) |
|  | EB | 690 | 30 (2) | 70 (3) | 30 (2) | 70 (3) |
|  | WB | 775 | 30 (2) | 75 (3) | 45 (2) | 100 (4) |
| SR 299/SR 3 | NB | 225 | 65 (3) | 180 (8) | 80 (4) | 200 (8) |
|  | SB | 530 | 40 (2) | 95 (4) | 50 (2) | 145 (6) |
|  | WB | 280 | 35 (2) | 80 (4) | 40 (2) | 95 (4) |
| SR 299/Garden Gulch Street | NB | 230 | 15 (1) | 60 (3) | 25 (1) | 80 (4) |
|  | SB | 175 | 30 (2) | 80 (4) | 35 (2) | 95 (4) |
|  | EB | 295 | 15 (1) | 50 (2) | 20 (1) | 70 (3) |
|  | WB | 1230 | 10 (1) | 55 (3) | 15 (1) | 60 (3) |

Notes: ${ }^{1}$ Distance estimated using Google Maps.
${ }^{2}$ The vehicle queue length was calculated assuming an average car length of 25 feet. A queue length of 5-25 feet is considered one vehicle, $26-50$ feet is two vehicles, etc. The queuing results are also a product of a simulation that is designed to represent "real-life" drivers to the best extent possible. Therefore, each simulation run represents a unique set of data. An average of 10 runs is shown in the results table.
${ }^{3}$ This is the distance to Fairway Drive. Nugget Lane is marked "Keep Clear" and was therefore excluded. Analysis performed assuming the SR 299 corridor is the North-South direction.
Source: Fehr \& Peers, 2011
The vehicle queues on SR 299 are not expected to spill back into adjacent intersections. Vehicle queues at the study intersections are only expected during the peak traffic periods and dissipate quickly.

## Travel Time Through Corridor

Travel time through the SR 299 corridor was analyzed for 2009 conditions and 2040 conditions (with East Connector). Table 12 shows the results and the technical analysis is provided in the Attachment D.

TABLE 12
TRAVEL TIME THROUGH SR 299 CORRIDOR (WITH SIGNALS AND ROUNDABOUTS)

| Direction of Travel | Travel Time |  |
| :---: | :---: | :---: |
|  | $\mathbf{2 0 0 9}$ Conditions <br> (with East Connector) | $\mathbf{2 0 4 0}$ Conditions <br> (with East Connector) |
| Northbound | 4.2 minutes | 4.3 minutes |
| Southbound | 4.0 minutes | 4.1 minutes |

Notes: The analysis includes the section of SR 299 between the SR 299/Martin Street and SR 299/Garden Gulch StreetForest Avenue intersections.
Source: Fehr \& Peers, 2011
The total travel time through the corridor, with traffic signals and roundabouts at the study intersections, is approximately 4 minutes, which is an increase of $1 / 2-1$ minute over the existing travel time.

## Greenhouse Gas Emissions

Greenhouse gas emissions were analyzed using Synchro software. Carbon monoxide, nitrogen oxides, volatile organic compound emissions were analyzed at the study intersections. The emissions results are shown in Table 13. The technical analysis is provided in the Attachment D.

| TABLE 13 <br> GREENHOUSE GAS EMISSIONS RESULTS (WITH SIGNALS AND ROUNDABOUTS) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Emissions ${ }^{1}$ |  |  |  |  |  |
|  | 2009 Conditions (with East Connector) |  |  | 2040 Conditions (with East Connector) |  |  |
|  | co | $\mathrm{NO}_{\mathrm{x}}$ | voc | co | $\mathrm{NO}_{\mathrm{x}}$ | voc |
| SR 299/Glen Road-East Connector | 1.03 | 0.20 | 0.24 | 1.15 | 0.22 | 0.27 |
| SR 299/Washington Street | 0.56 | 0.11 | 0.13 | 0.87 | 0.17 | 0.20 |
| SR 299/SR 3 | 0.50 | 0.10 | 0.12 | 0.65 | 0.13 | 0.15 |
| SR 299/Garden Gulch Street | 0.60 | 0.12 | 0.14 | 0.71 | 0.14 | 0.17 |
| Notes: ${ }^{1} \mathrm{CO}=$ Carbon Monoxide, $\mathrm{NO}_{\mathrm{x}}=$ Nitrogen Oxides, $\mathrm{VOC}=$ Volatile Organic Compounds Emissions reported in kilograms (for the peak hour). <br> Source: Fehr \& Peers, 2011 |  |  |  |  |  |  |

The 2009 conditions (with East Connector) greenhouse gas emissions increase at some intersections and decrease at some intersections compared to existing conditions analysis results because the traffic volumes at the intersections change due to the East Connector. Therefore, the existing conditions and 2009 conditions (with East Connector) analysis results cannot be compared directly because the scenarios do not share a common baseline.

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The 2040 conditions (with East Connector) with signalized intersections emissions results increase at all of the study intersections compared to the 2040 conditions with unsignalized intersections emissions results. The traffic volumes at the study intersections were the same for both scenarios. The traffic signals increased the emissions at the study intersections by small amounts (less than 0.20 kilograms). The emissions increase at the study intersections with roundabouts because a roundabout control reduces the speed of approaching vehicles causing vehicles to brake as they enter and accelerate as they exit a roundabout. Without a roundabout, the through movements on SR 299 are freely flowing and do not have to decelerate or accelerate at intersections.

## SUMMARY OF CORRIDOR ANALYSIS RESULTS

Table 14 shows a summary of the level of service results at the study intersections assuming different traffic controls.

Table 15 shows the travel time results through the SR 299 corridor for the three analysis scenarios: unsignalized intersections (existing conditions), signalized intersections (2009 conditions with the East Connector and 2040 conditions with the East Connector), and signalized and roundabout intersections (2009 conditions with the East Connector and 2040 conditions with the East Connector).

Table 16 shows the greenhouse gas emissions analysis results. The existing conditions analysis results, along with the 2009 conditions (with East Connector) and 2040 conditions (with East Connector) analysis results with signalized and roundabout controls are shown.

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TABLE 14
LEVEL OF SERVICE SUMMARY TABLE

| Intersection | Control Type ${ }^{1}$ | Existing Conditions |  | 2009 Conditions (with East Connector) |  | 2040 Conditions (with East Connector) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS |
| SR 299/Glen Road-East Connector | SSSC | 24.7 | C | 42.8 | E | 80.3 | F |
|  | Signal | -- | -- | 13.7 | B | 13.9 | B |
|  | Roundabout |  |  | 9.1 | A | 9.5 | A |
| SR 299/Washington Street | SSSC | 44.0 | E | 27.8 | D | 128.1 | F |
|  | Signal | -- | -- | 10.3 | B | 11.9 | B |
| SR 299/SR 3 | SSSC | 16.7 | C | 17.2 | C | 15.7 | C |
|  | Signal | -- | -- | 10.4 | B | 11.6 | B |
| SR 299/Garden Gulch Street | SSSC | 20.9 | C | 22.9 | C | 29.7 | D |
|  | Signal | -- | -- | 11.8 | B | 15.3 | B |
|  | Roundabout |  |  | 7.6 | A | 7.9 | A |

Notes: ${ }^{1}$ SSSC = Side Street Stop Control
${ }^{2}$ Delay is reported in seconds per vehicle for the overall intersection for signalized and roundabout intersections, and the worst movement for unsignalized intersections.
Source: Fehr \& Peers, 2011

TABLE 15
TRAVEL TIME SUMMARY TABLE

| Direction of <br> Travel | Existing Conditions | 2009 Conditions <br> (with East Connector) |  | 2040 Conditions <br> (with East Connector) |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | Unsignalized <br> Intersections | Signalized <br> Intersections | Signalized and <br> Roundabout Intersections | Signalized <br> Intersections | Signalized and <br> Roundabout Intersections |
|  | 2.9 minutes | 4.2 minutes | 4.2 minutes | 4.3 minutes | 4.3 minutes |
| Southbound | 3.4 minutes | 3.8 minutes | 4.0 minutes | 3.9 minutes | 4.1 minutes |

Notes: ${ }^{1}$ Signals or roundabouts will be added with the East Connector which will increase the travel time through the SR 299 corridor.
The analysis includes the section of SR 299 between the SR 299/Martin Street and SR 299/Garden Gulch Street - Forest Avenue intersections.
Source: Fehr \& Peers, 2011
Adding signals or roundabouts to the study intersections increases the travel time through the SR 299 corridor by approximately $1 / 2$ minute to $1 \frac{1}{2}$ minutes depending on the direction of travel. The difference in travel time between 2009 conditions and 2040 conditions is 0.1 minutes.

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TABLE 16
GREENHOUSE GAS EMISSIONS SUMMARY TABLE

| Intersection | Existing Conditions <br> Unsignalized Intersections |  |  | 2009 Conditions (with East Connector) |  |  |  |  |  | 2040 Conditions (with East Connector) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Signalized Intersections |  |  | Signalized and Roundabout Intersections |  |  | Unsignalized Intersections |  |  | Signalized Intersections |  |  | Signalized and Roundabout Intersections |  |  |
|  | CO | $\mathrm{NO}_{\text {x }}$ | VOC | CO | $\mathrm{NO}_{\mathrm{x}}$ | Voc | CO | $\mathrm{NO}_{\mathrm{x}}$ | VOC | CO | NOX | VOC | CO | $\mathrm{NO}_{\mathrm{x}}$ | VOC | CO | NOX | VOC |
| SR 299/Glen Road-East Connector | 1.02 | 0.20 | 0.24 | 1.01 | 0.20 | 0.23 | 1.03 | 0.20 | 0.24 | 1.13 | 0.22 | 0.26 | 1.14 | 0.22 | 0.27 | 1.15 | 0.22 | 0.27 |
| SR 299/ Washington Street | 1.40 | 0.27 | 0.33 | 0.56 | 0.11 | 0.13 | 0.56 | 0.11 | 0.13 | 0.74 | 0.14 | 0.17 | 0.88 | 0.17 | 0.20 | 0.87 | 0.17 | 0.20 |
| SR 299/SR 3 | 0.80 | 0.16 | 0.19 | 0.50 | 0.10 | 0.12 | 0.50 | 0.10 | 0.12 | 0.50 | 0.10 | 0.12 | 0.65 | 0.13 | 0.15 | 0.65 | 0.13 | 0.15 |
| SR 299/Garden Gulch Street | 0.52 | 0.10 | 0.12 | 0.58 | 0.11 | 0.13 | 0.60 | 0.12 | 0.14 | 0.58 | 0.11 | 0.13 | 0.70 | 0.14 | 0.16 | 0.71 | 0.14 | 0.17 |

Notes: ${ }^{1} \mathrm{CO}=$ Carbon Monoxide, $\mathrm{NO}_{\mathrm{x}}=$ Nitrogen Oxides, $\mathrm{VOC}=$ Volatile Organic Compounds
Source: Fehr \& Peers, 2011

The analysis results show that signals and roundabout will increase emissions at the study intersections, but by a very small amount. Traffic congestion along SR 299 through Weaverville is minimal; therefore there is little difference in emissions at a traffic signal versus a roundabout.

## CENTER STREET CONVERSION ANALYSIS

Analysis was performed to determine the effects of converting Center Street between Court Street and SR 3 from a one-way section to a two-way section. Traffic operations at the SR 299/SR 3 intersection were analyzed. The Trinity County travel demand model and daily roadway segment traffic volumes provided by the County were used to determine initial traffic volume estimates on Center Street, and SR 3, SR 299, and Court Street adjacent to Center Street.

Traffic volumes on Center Street and the surrounding roadway network were adjusted assuming Center Street is converted from a one-way section to a two-way section. Table 17 shows the change in delay and level of service at the SR 299/SR 3 intersection based on a shift in traffic to Center Street. The technical calculations are provided in Attachment F.

| TABLE 17CENTER STREET CONVERSION LOS RESULTS - SR 299/SR 3 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Scenario | Without Conversion (One-Way Section) |  | With Conversion (Two-Way Section) |  |
|  | Delay ${ }^{1}$ | LOS | Delay ${ }^{1}$ | LOS |
| Existing Conditions | 16.7 | C | 16.6 | C |
| 2009 (with East Connector) | 17.2 | C | 14.4 | C |
| 2040 (with East Connector) | 15.7 | C | 15.7 | C |
| Notes: ${ }^{1}$ Delay is reported in seconds per vehicle for worst movement for unsignalized intersections. <br> Source: Fehr \& Peers, 2011 |  |  |  |  |

As shown in the table, the delay at the SR 299/SR 3 intersection is expected to decrease or stay the same if Center Street is converted to a two-way section.

The daily roadway segment traffic volumes were analyzed based on a shift in traffic to Center Street. Center Street currently carries 700-800 daily trips and is a one way street. Converting Center Street to two-way operations will shift approximately 500-600 daily trips from State Route 299 (between SR 3 and Court Street in Downtown Weaverville) to Center Street. The study segment of Center Street is expected to carry $1,200-1,300$ daily trips, and operate at LOS B as a two-way section. The daily LOS on SR 299 between SR 3 and Court Street in Downtown Weaverville would remain at the current level.

## CONCLUSIONS AND RECOMMENDATIONS

Scenario 1: Unsignalized Intersections

- The SR 299/Washington Street intersection currently operates at an unacceptable level of service.
- When the East Connector is constructed, traffic is expected to shift from Washington Street to the East Connector, improving the level of service at the SR 299/Washington

Street intersection, but diminishing the level of service at the SR 299/Glen Road-East Connector intersection under 2009 conditions (with East Connector).

- The SR 299/Glen Road-East Connector and SR 299/Washington Street intersections will operate at unacceptable levels of service under 2040 conditions (with East Connector) with unsignalized intersections.
- The travel time through the SR 299 corridor is approximately 3 to $31 / 2$ minutes with unsignalized intersections.

Scenario 2: Signalized Intersections

- The study intersections are expected to operate at LOS B with traffic signals.
- Queue lengths are not expected to exceed storage lengths or spill back into upstream intersections.
- The travel time through the corridor is expected to increase by $1 / 2-1 \frac{1}{2}$ minute compared to existing conditions.
- The 2040 conditions greenhouse gas emissions analysis compared the results of the unsignalized intersections to the signalized intersections. The results show that signalized intersections will increase emissions along SR 299, but by a small amount (less than 0.20 kilograms).
- The Traffic Vibration Assessment (provided in Attachment E) indicates that installing traffic signals at the study intersections will not significantly increase roadway vibration along the SR 299 corridor.

Scenario 3: Signalized and Roundabout Intersections

- The study intersections are expected to operate at LOS B or better with traffic signals and roundabouts. (Roundabouts at the SR 299/Glen Road-East Connector and SR 299/Garden Gulch Street intersections.)
- Queue lengths are not expected to exceed storage lengths or spill back into upstream intersections.
- The travel time through the corridor is expected to increase by $1 / 2-1 \frac{1}{2}$ minute compared to existing conditions.
- The 2040 conditions greenhouse gas emissions analysis compares the results of the unsignalized intersections to the signalized and roundabout intersections. The results show that signalized and roundabout intersections will increase emissions along SR 299, but by a small amount (less than 0.20 kilograms). The comparison of signals to roundabouts at the study intersections is negligible. The production of emissions at the study intersections is virtually the same with a roundabout or a signal.

Overall, the analysis indicates that a system of traffic signals or a combination of traffic signals and roundabouts will function well.

## Center Street Conversion

- The daily LOS on SR 299 between SR 3 and Court Street in Downtown Weaverville would remain at the current level.
- The delay at the SR 299/SR 3 intersection is expected to decrease or stay the same if Center Street is converted from a one-way section to a two-way section (under existing and 2040 conditions).
- The Center Street roadway segment between Court Street and SR 3 is expected to operate at LOS B as a two-way section (it currently operates at LOS B as a one-way segment).

Based on the analysis, we recommend:

- A traffic signal or roundabout should be installed at the SR 299/Glen Road-East Connector intersection when the East Connector roadway is constructed.
- A traffic signal should be installed at the SR 299/Washington Street intersection when traffic volumes and level of service indicate the need (anticipated in the 10-20 year timeframe).
- A traffic signal or roundabout should be constructed at the SR 299/Garden Gulch intersection when traffic volumes and level of service indicate the need (anticipated in 1020 year timeframe).

We appreciate the opportunity to assist Trinity County with this project. Please feel free to call if you have any questions (775) 826-3200.

Sincerely,
FEHR \& PEERS


Katy Cole, P.E.
Marissa Harned
Associate
Transportation Planner

RN09-0427
Attachments
A - Signal Warrant Analysis
B - Scenario 1: Unsignalized Intersections
C - Scenario 2: Signalized Intersections
D - Scenario 3: Signalized and Roundabout Intersections

E - Traffic Vibration Assessment: Trinity County Intersection Improvements (Bollard Acoustical Consultants, Inc.)
F - Center Street Conversion Analysis

ATTACHMENT A
SIGNAL WARRANT ANALYSIS

TRAFFIC SIGNAL WARRANTS
FOUR HOUR VEHICULAR VOLUME (MUTCD Warrant 2, Caltrans Warrant 9) PEAK HOUR VEHICULAR VOLUME (MUTCD Warrant 3, Caltrans Warrant 11)


Notes:
a. May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000 .
b. Heavier left-turn movement from the major street may be included with minor street volume if a separate signal phase is proposed for left-turn movements.
c. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-2.
d. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-4.

Adopted from: U.S. Department of Transportation, Federal Highway Administration, "Manual on Uniform Traffic Control Devices, Millennium Edition," 2001; and Caltrans, "Traffic Manual," 2002.

TRAFFIC SIGNAL WARRANTS
FOUR HOUR VEHICULAR VOLUME (MUTCD Warrant 2, Caltrans Warrant 9) PEAK HOUR VEHICULAR VOLUME (MUTCD Warrant 3, Caltrans Warrant 11)


Notes:
a. May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000 .
b. Heavier left-turn movement from the major street may be included with minor street volume if a separate signal phase is proposed for left-turn movements.
c. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-2.
d. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-4.

Adopted from: U.S. Department of Transportation, Federal Highway Administration, "Manual on Uniform Traffic Control Devices, Millennium Edition," 2001; and Caltrans, "Traffic Manual," 2002.

TRAFFIC SIGNAL WARRANTS
FOUR HOUR VEHICULAR VOLUME (MUTCD Warrant 2, Caltrans Warrant 9) PEAK HOUR VEHICULAR VOLUME (MUTCD Warrant 3, Caltrans Warrant 11)


Notes:
a. May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000 .
b. Heavier left-turn movement from the major street may be included with minor street volume if a separate signal phase is proposed for left-turn movements.
c. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-2.
d. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-4.

Adopted from: U.S. Department of Transportation, Federal Highway Administration, "Manual on Uniform Traffic Control Devices, Millennium Edition," 2001; and Caltrans, "Traffic Manual," 2002.

TRAFFIC SIGNAL WARRANTS
FOUR HOUR VEHICULAR VOLUME (MUTCD Warrant 2, Caltrans Warrant 9) PEAK HOUR VEHICULAR VOLUME (MUTCD Warrant 3, Caltrans Warrant 11)


Notes:
a. May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000 .
b. Heavier left-turn movement from the major street may be included with minor street volume if a separate signal phase is proposed for left-turn movements.
c. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-2.
d. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-4.

Adopted from: U.S. Department of Transportation, Federal Highway Administration, "Manual on Uniform Traffic Control Devices, Millennium Edition," 2001; and Caltrans, "Traffic Manual," 2002.

TRAFFIC SIGNAL WARRANTS
FOUR HOUR VEHICULAR VOLUME (MUTCD Warrant 2, Caltrans Warrant 9) PEAK HOUR VEHICULAR VOLUME (MUTCD Warrant 3, Caltrans Warrant 11)

| Major Street: SR 299  <br> Minor Street: East Connector  <br> Scenario: 2040  <br> Urban/Rural: $r \quad$ (U=urban, R=rural [a])  |  |  |  |
| :---: | :---: | :---: | :---: |
| FOUR HOUR VOLUME (MUTCD Warrant 2, Caltrans Warrant 9) |  |  |  |
| Number of Lanes on Each Approach Major Street: <br> Minor Street: | 1 1 |  |  |
| Vehicles Per Hour (4th Highest Hour) |  |  |  |
| Major Street (Approach 1): | 417 | Major Street Left Turn (see note [b]): | 0 |
| Major Street (Approach 2): | 374 | Minor Street (Higher Volume App.): | 136 |
| Major Street Total (Both Approaches): | 791 | Minor Street Total: | 136 |
| Minimum Volume on Major Street to Satisfy Warrant (see note [c]): | 270 | Minimum Volume on Minor Street to Satisfy Warrant (see note [c]): | 60 |
| FOUR HOUR VOLUME WARRANT SATISFIED? |  |  |  |
| PEAK HOUR VOLUME (MUTCD Warrant 3, Caltrans Warrant 11) |  |  |  |
| Number of Lanes on Each Approach |  |  |  |
| Major Street: | 1 |  |  |
| Minor Street: | 1 |  |  |
| Vehicles Per Hour (Peak Hour) |  |  |  |
| Major Street (Approach 1): | 490 | Major Street Left Turn (see note [b]): | 0 |
| Major Street (Approach 2): | $\underline{440}$ | Minor Street (Higher Volume App.): | 160 |
| Major Street Total (Both Approaches): | 930 | Minor Street Total: | 160 |
| Minimum Volume on Major Street to Satisfy Warrant (see note [d]): | 310 | Minimum Volume on Minor Street to Satisfy Warrant (see note [d]): | 90 |
| PEAK HOUR VOLUME WARRANT SATISFIED? |  |  |  |

Notes:
a. May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000 .
b. Heavier left-turn movement from the major street may be included with minor street volume if a separate signal phase is proposed for left-turn movements.
c. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-2.
d. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-4.

Adopted from: U.S. Department of Transportation, Federal Highway Administration, "Manual on Uniform Traffic Control Devices, Millennium Edition," 2001; and Caltrans, "Traffic Manual," 2002.

TRAFFIC SIGNAL WARRANTS
FOUR HOUR VEHICULAR VOLUME (MUTCD Warrant 2, Caltrans Warrant 9) PEAK HOUR VEHICULAR VOLUME (MUTCD Warrant 3, Caltrans Warrant 11)


Notes:
a. May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000 .
b. Heavier left-turn movement from the major street may be included with minor street volume if a separate signal phase is proposed for left-turn movements.
c. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-2.
d. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-4.

Adopted from: U.S. Department of Transportation, Federal Highway Administration, "Manual on Uniform Traffic Control Devices, Millennium Edition," 2001; and Caltrans, "Traffic Manual," 2002.

TRAFFIC SIGNAL WARRANTS
FOUR HOUR VEHICULAR VOLUME (MUTCD Warrant 2, Caltrans Warrant 9) PEAK HOUR VEHICULAR VOLUME (MUTCD Warrant 3, Caltrans Warrant 11)


Notes:
a. May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000 .
b. Heavier left-turn movement from the major street may be included with minor street volume if a separate signal phase is proposed for left-turn movements.
c. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-2.
d. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-4.

Adopted from: U.S. Department of Transportation, Federal Highway Administration, "Manual on Uniform Traffic Control Devices, Millennium Edition," 2001; and Caltrans, "Traffic Manual," 2002.

TRAFFIC SIGNAL WARRANTS
FOUR HOUR VEHICULAR VOLUME (MUTCD Warrant 2, Caltrans Warrant 9) PEAK HOUR VEHICULAR VOLUME (MUTCD Warrant 3, Caltrans Warrant 11)

| Major Street: SR 299  <br> Minor Street: Garden Gultch  <br> Mcenario: 2040  <br> Urban/Rural: $r \quad$ (U=urban, R=rural [a])  |  |  |  |
| :---: | :---: | :---: | :---: |
| FOUR HOUR VOLUME (MUTCD Warrant 2, Caltrans Warrant 9) |  |  |  |
| Number of Lanes on Each Approach |  |  |  |
| Major Street: | 1 |  |  |
| Minor Street: | 1 |  |  |
| Vehicles Per Hour (4th Highest Hour) |  |  |  |
| Major Street (Approach 1): | 323 | Major Street Left Turn (see note [b]): | 0 |
| Major Street (Approach 2): | $\underline{247}$ | Minor Street (Higher Volume App.): | 77 |
| Major Street Total (Both Approaches): | 570 | Minor Street Total: | 77 |
| Minimum Volume on Major Street to Satisfy Warrant (see note [c]): | 270 | Minimum Volume on Minor Street to Satisfy Warrant (see note [c]): | 110 |
| FOUR HOUR VOLUME WARRANT SATISFIED? |  |  |  |
| PEAK HOUR VOLUME (MUTCD Warrant 3, Caltrans Warrant 11) |  |  |  |
| Number of Lanes on Each Approach |  |  |  |
| Major Street: | 1 |  |  |
| Minor Street: | 1 |  |  |
| Vehicles Per Hour (Peak Hour) |  |  |  |
| Major Street (Approach 1): | 380 | Major Street Left Turn (see note [b]): | 0 |
| Major Street (Approach 2): | $\underline{290}$ | Minor Street (Higher Volume App.): | 90 |
| Major Street Total (Both Approaches): | 670 | Minor Street Total: | 90 |
| Minimum Volume on Major Street to Satisfy Warrant (see note [d]): | 310 | Minimum Volume on Minor Street to Satisfy Warrant (see note [d]): | 150 |
| PEAK HOUR VOLUME WARRANT SATISFIED? |  |  |  |

Notes:
a. May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000 .
b. Heavier left-turn movement from the major street may be included with minor street volume if a separate signal phase is proposed for left-turn movements.
c. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-2.
d. From: USDOT, FHWA, "Manual on Uniform Traffic Control Devices," 2001, Figure 4C-4.

Adopted from: U.S. Department of Transportation, Federal Highway Administration, "Manual on Uniform Traffic Control Devices, Millennium Edition," 2001; and Caltrans, "Traffic Manual," 2002.

## ATTACHMENT B <br> SCENARIO 1: UNSIGNALIZED INTERSECTIONS

|  | $\stackrel{ }{ }$ |  | 4 | $\dagger$ |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | M |  | \% | 4 | ¢ |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |
| Volume (veh/h) | 112 | 29 | 34 | 378 | 352 | 71 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |
| Hourly flow rate (vph) | 122 | 32 | 37 | 411 | 383 | 77 |  |
| Pedestrians |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type | None |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC , conflicting volume | 906 | 421 | 460 |  |  |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 906 | 421 | 460 |  |  |  |  |
| tC, single (s) | 6.4 | 6.2 | 4.1 |  |  |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 | 2.2 |  |  |  |  |
| p0 queue free \% | 59 | 95 | 97 |  |  |  |  |
| cM capacity (veh/h) | 296 | 632 | 1101 |  |  |  |  |
| Direction, Lane \# | EB 1 | NB 1 | NB 2 | SB 1 |  |  |  |
| Volume Total | 153 | 37 | 411 | 460 |  |  |  |
| Volume Left | 122 | 37 | 0 | 0 |  |  |  |
| Volume Right | 32 | 0 | 0 | 77 |  |  |  |
| cSH | 333 | 1101 | 1700 | 1700 |  |  |  |
| Volume to Capacity | 0.46 | 0.03 | 0.24 | 0.27 |  |  |  |
| Queue Length 95th (ft) | 58 | 3 | 0 | 0 |  |  |  |
| Control Delay (s) | 24.7 | 8.4 | 0.0 | 0.0 |  |  |  |
| Lane LOS | C | A |  |  |  |  |  |
| Approach Delay (s) | 24.7 | 0.7 |  | 0.0 |  |  |  |
| Approach LOS C |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 3.9 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 42.9\% | ICU Level of Service |  |  | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |







|  | 7 |  | $\dagger$ | $p$ |  | $\dagger$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | \% | $\stackrel{7}{ }$ | $\uparrow$ |  | * | $\uparrow$ |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Grade | 0\% |  | 6\% |  |  | -6\% |  |
| Volume (veh/h) | 70 | 80 | 220 | 90 | 70 | 210 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.87 | 0.87 | 0.86 | 0.86 |  |
| Hourly flow rate (vph) | 77 | 88 | 253 | 103 | 81 | 244 |  |
| Pedestrians |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type | None |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |
| pX , platoon unblocked |  |  |  |  |  |  |  |
| vC, conflicting volume | 712 | 305 |  |  | 356 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 712 | 305 |  |  | 356 |  |  |
| tC, single (s) | 6.4 | 6.2 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 |  |  | 2.2 |  |  |
| p0 queue free \% | 79 | 88 |  |  | 93 |  |  |
| cM capacity (veh/h) | 372 | 735 |  |  | 1202 |  |  |
| Direction, Lane \# | WB 1 | WB 2 | NB 1 | SB 1 | SB 2 |  |  |
| Volume Total | 77 | 88 | 356 | 81 | 244 |  |  |
| Volume Left | 77 | 0 | 0 | 81 | 0 |  |  |
| Volume Right | 0 | 88 | 103 | 0 | 0 |  |  |
| cSH | 372 | 735 | 1700 | 1202 | 1700 |  |  |
| Volume to Capacity | 0.21 | 0.12 | 0.21 | 0.07 | 0.14 |  |  |
| Queue Length 95th (ft) | 19 | 10 | 0 | 5 | 0 |  |  |
| Control Delay (s) | 17.2 | 10.6 | 0.0 | 8.2 | 0.0 |  |  |
| Lane LOS | C | B |  | A |  |  |  |
| Approach Delay (s) | 13.6 |  | 0.0 | 2.1 |  |  |  |
| Approach LOS | B |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 3.4 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 34.8\% | ICU Level of Service |  |  | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |







## Arterial Level of Service: NB SR 299

| Cross Street | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Martin Lane | 0.8 | 13.2 | 0.1 | 29 |
|  | 1.4 | 27.2 | 0.2 | 28 |
| Washington Street | 2.5 | 31.8 | 0.2 | 27 |
|  | 3.2 | 27.7 | 0.2 | 32 |
| SR 3 | 2.2 | 26.0 | 0.2 | 26 |
|  | 3.9 | 29.2 | 0.2 | 29 |
| Garden Gulch | 1.4 | 14.1 | 0.1 | 25 |
| Total | 1.0 | 6.7 | 0.0 | 26 |

Arterial Level of Service: SB SR 299

| Cross Street | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Forest Ave | 2.1 | 43.8 | 0.3 | 29 |
| SR 3 | 0.5 | 6.6 | 0.0 | 27 |
|  | 0.8 | 11.8 | 0.1 | 30 |
|  | 1.9 | 30.3 | 0.2 | 27 |
|  | 2.3 | 22.1 | 0.2 | 32 |
| Martin Lane | 3.3 | 33.0 | 0.2 | 26 |
| Total | 4.1 | 33.5 | 0.2 | 26 |

## Arterial Level of Service: NB SR 299

| Cross Street | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Martin Road | 1.2 | 18.9 | 0.1 | 29 |
|  | 1.3 | 21.1 | 0.2 | 28 |
| East Connector Road | 1.1 | 7.4 | 0.1 | 30 |
| Washington Street | 2.4 | 31.8 | 0.2 | 27 |
|  | 3.2 | 30.5 | 0.2 | 28 |
| SR 3 | 2.9 | 27.0 | 0.2 | 25 |
|  | 4.4 | 30.3 | 0.2 | 27 |
| Garden Gulch | 1.5 | 13.9 | 0.1 | 25 |
| Total | 1.1 | 6.9 | 0.0 | 26 |

Arterial Level of Service: SB SR 299

| Cross Street | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Forest Ave | 2.5 | 44.6 | 0.3 | 28 |
| SR 3 | 0.5 | 6.5 | 0.0 | 27 |
|  | 0.9 | 11.9 | 0.1 | 30 |
|  | 2.0 | 30.4 | 0.2 | 27 |
| Glen Road | 2.4 | 22.5 | 0.2 | 31 |
|  | 3.3 | 32.0 | 0.2 | 26 |
| Nugget Lane | 4.3 | 31.6 | 0.2 | 27 |
| Total | 0.9 | 8.2 | 0.1 | 26 |
|  | 1.6 | 19.2 | 0.2 | 30 |

## Arterial Level of Service: NB SR 299

| Cross Street | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Martin Road | 1.3 | 17.4 | 0.1 | 29 |
| East Connector Road | 1.0 | 15.7 | 0.1 | 27 |
| Washington Street | 1.4 | 8.3 | 0.1 | 31 |
| SR 3 | 4.1 | 44.8 | 0.3 | 26 |
|  | 3.0 | 21.5 | 0.2 | 27 |
| Garden Gulch | 2.6 | 26.6 | 0.2 | 26 |
| Total | 4.2 | 29.9 | 0.2 | 28 |

Arterial Level of Service: SB SR 299

| Cross Street | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Forest Ave | 2.7 | 44.9 | 0.3 | 28 |
| SR 3 | 0.5 | 6.6 | 0.0 | 27 |
|  | 1.0 | 12.1 | 0.1 | 29 |
|  | 2.1 | 30.6 | 0.2 | 27 |
| Glen Road | 2.7 | 23.0 | 0.2 | 30 |
|  | 2.4 | 22.2 | 0.2 | 26 |
| Nugget Lane | 5.1 | 40.8 | 0.3 | 29 |
| Total | 1.1 | 9.4 | 0.1 | 26 |

1: Glen Road \& SR 299

| Direction | All |
| :--- | :---: |
| Volume (vph) | 977 |
| CO Emissions $(\mathrm{kg})$ | 1.02 |
| NOX Emissions $(\mathrm{kg})$ | 0.20 |
| VOC Emissions $(\mathrm{kg})$ | 0.24 |

2: Washington Street \& SR 299

| Direction | All |
| :--- | ---: |
| Volume $(\mathrm{vph})$ | 1001 |
| CO Emissions $(\mathrm{kg})$ | 1.40 |
| NOx Emissions $(\mathrm{kg})$ | 0.27 |
| VOC Emissions $(\mathrm{kg})$ | 0.33 |

3: SR 3 \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 719 |
| CO Emissions $(\mathrm{kg})$ | 0.80 |
| NOx Emissions $(\mathrm{kg})$ | 0.16 |
| VOC Emissions $(\mathrm{kg})$ | 0.19 |

4: Forest Ave \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 645 |
| CO Emissions $(\mathrm{kg})$ | 0.52 |
| NOx Emissions $(\mathrm{kg})$ | 0.10 |
| VOC Emissions $(\mathrm{kg})$ | 0.12 |

## 1: Glen Road \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 1210 |
| CO Emissions $(\mathrm{kg})$ | 1.13 |
| NOx Emissions $(\mathrm{kg})$ | 0.22 |
| VOC Emissions $(\mathrm{kg})$ | 0.26 |

2: Washington Street \& SR 299

| Direction | All |
| :--- | ---: |
| Volume $(\mathrm{vph})$ | 1171 |
| CO Emissions $(\mathrm{kg})$ | 0.74 |
| NOx Emissions $(\mathrm{kg})$ | 0.14 |
| VOC Emissions $(\mathrm{kg})$ | 0.17 |

3: SR 3 \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 880 |
| CO Emissions $(\mathrm{kg})$ | 0.50 |
| NOX Emissions $(\mathrm{kg})$ | 0.10 |
| VOC Emissions $(\mathrm{kg})$ | 0.12 |

4: Forest Ave \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 832 |
| CO Emissions $(\mathrm{kg})$ | 0.58 |
| NOX Emissions $(\mathrm{kg})$ | 0.11 |
| VOC Emissions $(\mathrm{kg})$ | 0.13 |

## ATTACHMENT C

## SCENARIO 2: SIGNALIZED INTERSECTIONS




c Critical Lane Group

|  | 4 |  |  |  |  |  | 4 | 4 |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | $\uparrow$ | 「 | \% | $\hat{\sim}$ |  | ${ }^{*}$ | $\hat{\beta}$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (\%) |  | 5\% |  |  | -5\% |  |  | 0\% |  |  | 4\% |  |
| Total Lost time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| Lane Util. Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frt |  | 1.00 | 0.85 |  | 1.00 | 0.85 | 1.00 | 0.97 |  | 1.00 | 0.99 |  |
| Flt Protected |  | 0.98 | 1.00 |  | 0.96 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) |  | 1772 | 1544 |  | 1836 | 1623 | 1770 | 1814 |  | 1734 | 1814 |  |
| Flt Permitted |  | 0.84 | 1.00 |  | 0.76 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (perm) |  | 1519 | 1544 |  | 1442 | 1623 | 1770 | 1814 |  | 1734 | 1814 |  |
| Volume (vph) | 10 | 10 | 50 | 40 | 10 | 10 | 80 | 190 | 40 | 10 | 230 | 10 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.74 | 0.74 | 0.74 | 0.84 | 0.84 | 0.84 | 0.83 | 0.84 | 0.83 |
| Adj. Flow (vph) | 11 | 11 | 56 | 54 | 14 | 14 | 95 | 226 | 48 | 12 | 274 | 12 |
| RTOR Reduction (vph) | 0 | 0 | 49 | 0 | 0 | 12 | 0 | 8 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 0 | 22 | 7 | 0 | 68 | 2 | 95 | 266 | 0 | 12 | 284 | 0 |
| Turn Type | Perm |  | Perm | Perm |  | Perm | Prot |  |  | Prot |  |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 |  |  |  |  |  |  |
| Actuated Green, G (s) |  | 6.7 | 6.7 |  | 6.7 | 6.7 | 5.7 | 37.6 |  | 1.0 | 32.9 |  |
| Effective Green, g (s) |  | 6.7 | 6.7 |  | 6.7 | 6.7 | 5.7 | 37.6 |  | 1.0 | 32.9 |  |
| Actuated g/C Ratio |  | 0.12 | 0.12 |  | 0.12 | 0.12 | 0.10 | 0.66 |  | 0.02 | 0.57 |  |
| Clearance Time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| Vehicle Extension (s) |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) |  | 178 | 181 |  | 169 | 190 | 176 | 1190 |  | 30 | 1042 |  |
| v/s Ratio Prot |  |  |  |  |  |  | c0.05 | 0.15 |  | 0.01 | c0.16 |  |
| v/s Ratio Perm |  | 0.01 | 0.00 |  | c0.05 | 0.00 |  |  |  |  |  |  |
| v/c Ratio |  | 0.12 | 0.04 |  | 0.40 | 0.01 | 0.54 | 0.22 |  | 0.40 | 0.27 |  |
| Uniform Delay, d1 |  | 22.7 | 22.4 |  | 23.4 | 22.4 | 24.6 | 4.0 |  | 27.9 | 6.2 |  |
| Progression Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 |  | 0.3 | 0.1 |  | 1.6 | 0.0 | 3.2 | 0.1 |  | 8.5 | 0.1 |  |
| Delay (s) |  | 23.0 | 22.5 |  | 25.0 | 22.4 | 27.7 | 4.1 |  | 36.4 | 6.3 |  |
| Level of Service |  | C | C |  | C | C | C | A |  | D | A |  |
| Approach Delay (s) |  | 22.6 |  |  | 24.6 |  |  | 10.2 |  |  | 7.5 |  |
| Approach LOS |  | C |  |  | C |  |  | B |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 11.8 |  | HCM Lev | vel of S | rvice |  | B |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.33 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 57.3 |  | Sum of lost time (s) |  |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 36.6\% | ICU Level of Service |  |  |  |  | A |  |  |  |
| Analysis Period (min) |  | 15 |  |  |  |  |  |  |  |  |  |  |

C Critical Lane Group

|  | 4 |  |  |  |  |  | 4 | 4 |  |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | F |  | $\uparrow$ | F | \% | 4 | 「 | \% | 4 | F |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 1.00 | 0.85 |  | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected |  | 0.96 | 1.00 |  | 0.96 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1794 | 1583 |  | 1791 | 1583 | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 |
| Flt Permitted |  | 0.70 | 1.00 |  | 0.66 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1302 | 1583 |  | 1231 | 1583 | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 |
| Volume (vph) | 100 | 30 | 30 | 80 | 20 | 20 | 40 | 360 | 90 | 30 | 350 | 60 |
| Peak-hour factor, PHF | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 |
| Adj. Flow (vph) | 118 | 35 | 35 | 94 | 24 | 24 | 47 | 424 | 106 | 35 | 412 | 71 |
| RTOR Reduction (vph) | 0 | 0 | 29 | 0 | 0 | 20 | 0 | 0 | 36 | 0 | 0 | 25 |
| Lane Group Flow (vph) | 0 | 153 | 6 | 0 | 118 | 4 | 47 | 424 | 70 | 35 | 412 | 46 |
| Turn Type | Perm |  | Perm | Perm |  | Perm | Prot |  | Perm | Prot |  | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 |  |  | 2 |  |  | 6 |
| Actuated Green, G (s) |  | 9.3 | 9.3 |  | 9.3 | 9.3 | 1.8 | 30.7 | 30.7 | 1.8 | 30.7 | 30.7 |
| Effective Green, g (s) |  | 9.3 | 9.3 |  | 9.3 | 9.3 | 1.8 | 30.7 | 30.7 | 1.8 | 30.7 | 30.7 |
| Actuated g/C Ratio |  | 0.17 | 0.17 |  | 0.17 | 0.17 | 0.03 | 0.57 | 0.57 | 0.03 | 0.57 | 0.57 |
| Clearance Time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 225 | 274 |  | 213 | 274 | 59 | 1063 | 903 | 59 | 1063 | 903 |
| v/s Ratio Prot |  |  |  |  |  |  | c0.03 | c0.23 |  | 0.02 | 0.22 |  |
| v/s Ratio Perm |  | c0.12 | 0.00 |  | 0.10 | 0.00 |  |  | 0.04 |  |  | 0.03 |
| v/c Ratio |  | 0.68 | 0.02 |  | 0.55 | 0.02 | 0.80 | 0.40 | 0.08 | 0.59 | 0.39 | 0.05 |
| Uniform Delay, d1 |  | 20.9 | 18.5 |  | 20.4 | 18.5 | 25.8 | 6.4 | 5.2 | 25.6 | 6.4 | 5.1 |
| Progression Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 8.2 | 0.0 |  | 3.1 | 0.0 | 51.1 | 0.2 | 0.0 | 15.0 | 0.2 | 0.0 |
| Delay (s) |  | 29.0 | 18.5 |  | 23.5 | 18.5 | 76.9 | 6.7 | 5.2 | 40.6 | 6.6 | 5.1 |
| Level of Service |  | C | B |  | C | B | E | A | A | D | A | A |
| Approach Delay (s) |  | 27.1 |  |  | 22.6 |  |  | 12.1 |  |  | 8.7 |  |
| Approach LOS |  | C |  |  | C |  |  | B |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 13.9 |  | HCM Lev | vel of Servir | rvice |  | B |  |  |  |
| HCM Average Control Delay HCM Volume to Capacity ratio |  |  | 0.48 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 53.8 |  | Sum of los | st time |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 46.1\% |  | ICU Leve | ef Ser | vice |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |


|  | 4 | $\rightarrow$ | $\checkmark$ | 4 |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | \& |  | ${ }^{7}$ | 4 | 「 | ${ }^{*}$ | $\uparrow$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Frt |  | 0.91 |  |  | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 |  |
| Flt Protected |  | 0.99 |  |  | 0.96 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  |
| Satd. Flow (prot) |  | 1682 |  |  | 1768 |  | 1770 | 1863 | 1583 | 1770 | 1850 |  |
| Flt Permitted |  | 0.94 |  |  | 0.78 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  |
| Satd. Flow (perm) |  | 1596 |  |  | 1442 |  | 1770 | 1863 | 1583 | 1770 | 1850 |  |
| Volume (vph) | 10 | 10 | 40 | 90 | 10 | 10 | 50 | 380 | 110 | 30 | 410 | 20 |
| Peak-hour factor, PHF | 0.73 | 0.73 | 0.73 | 0.70 | 0.70 | 0.70 | 0.87 | 0.87 | 0.87 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 14 | 14 | 55 | 129 | 14 | 14 | 57 | 437 | 126 | 33 | 456 | 22 |
| RTOR Reduction (vph) | 0 | 43 | 0 | 0 | 5 | 0 | 0 | 0 | 59 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 0 | 40 | 0 | 0 | 152 | 0 | 57 | 437 | 67 | 33 | 476 | 0 |
| Turn Type | Perm |  |  | Perm |  |  | Prot |  | Perm | Prot |  |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  |  |  | 2 |  |  |  |
| Actuated Green, G (s) |  | 11.6 |  |  | 11.6 |  | 3.0 | 27.1 | 27.1 | 2.6 | 26.7 |  |
| Effective Green, g (s) |  | 11.6 |  |  | 11.6 |  | 3.0 | 27.1 | 27.1 | 2.6 | 26.7 |  |
| Actuated g/C Ratio |  | 0.22 |  |  | 0.22 |  | 0.06 | 0.51 | 0.51 | 0.05 | 0.50 |  |
| Clearance Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) |  | 347 |  |  | 314 |  | 100 | 947 | 805 | 86 | 927 |  |
| v/s Ratio Prot |  |  |  |  |  |  | c0.03 | 0.23 |  | 0.02 | c0.26 |  |
| v/s Ratio Perm |  | 0.03 |  |  | c0.11 |  |  |  | 0.04 |  |  |  |
| v/c Ratio |  | 0.12 |  |  | 0.48 |  | 0.57 | 0.46 | 0.08 | 0.38 | 0.51 |  |
| Uniform Delay, d1 |  | 16.7 |  |  | 18.2 |  | 24.5 | 8.4 | 6.7 | 24.6 | 8.9 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Incremental Delay, d2 |  | 0.1 |  |  | 1.2 |  | 7.3 | 0.4 | 0.0 | 2.8 | 0.5 |  |
| Delay (s) |  | 16.9 |  |  | 19.4 |  | 31.8 | 8.8 | 6.8 | 27.4 | 9.4 |  |
| Level of Service |  | B |  |  | B |  | C | A | A | C | A |  |
| Approach Delay (s) |  | 16.9 |  |  | 19.4 |  |  | 10.5 |  |  | 10.6 |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 11.9 |  | HCM Lev | el of S | ervice |  | B |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.51 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 53.3 |  | Sum of lo | st time |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 48.9\% |  | CU Leve | of Servir | vice |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |


c Critical Lane Group

|  | 4 |  |  |  |  |  | 4 | $\dagger$ |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | F |  | $\uparrow$ | 「 | \% | $\hat{\beta}$ |  | \% | $\hat{\beta}$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (\%) |  | 5\% |  |  | -5\% |  |  | 0\% |  |  | 4\% |  |
| Total Lost time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| Lane Util. Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frt |  | 1.00 | 0.85 |  | 1.00 | 0.85 | 1.00 | 0.97 |  | 1.00 | 0.99 |  |
| Flt Protected |  | 0.97 | 1.00 |  | 0.96 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) |  | 1758 | 1544 |  | 1833 | 1623 | 1770 | 1814 |  | 1734 | 1816 |  |
| Flt Permitted |  | 0.77 | 1.00 |  | 0.74 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (perm) |  | 1395 | 1544 |  | 1412 | 1623 | 1770 | 1814 |  | 1734 | 1816 |  |
| Volume (vph) | 20 | 10 | 60 | 50 | 10 | 10 | 90 | 240 | 50 | 10 | 270 | 10 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.74 | 0.74 | 0.74 | 0.84 | 0.84 | 0.84 | 0.83 | 0.84 | 0.83 |
| Adj. Flow (vph) | 22 | 11 | 67 | 68 | 14 | 14 | 107 | 286 | 60 | 12 | 321 | 12 |
| RTOR Reduction (vph) | 0 | 0 | 59 | 0 | 0 | 12 | 0 | 9 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 0 | 33 | 8 | 0 | 82 | 2 | 107 | 337 | 0 | 12 | 331 | 0 |
| Turn Type | Perm |  | Perm | Perm |  | Perm | Prot |  |  | Prot |  |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 |  |  |  |  |  |  |
| Actuated Green, G (s) |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 4.0 | 35.8 |  | 1.0 | 32.8 |  |
| Effective Green, g (s) |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 4.0 | 35.8 |  | 1.0 | 32.8 |  |
| Actuated g/C Ratio |  | 0.13 | 0.13 |  | 0.13 | 0.13 | 0.07 | 0.64 |  | 0.02 | 0.59 |  |
| Clearance Time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| Vehicle Extension (s) |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) |  | 175 | 194 |  | 177 | 204 | 127 | 1164 |  | 31 | 1067 |  |
| v/s Ratio Prot |  |  |  |  |  |  | c0.06 | c0.19 |  | 0.01 | 0.18 |  |
| v/s Ratio Perm |  | 0.02 | 0.01 |  | c0.06 | 0.00 |  |  |  |  |  |  |
| v/c Ratio |  | 0.19 | 0.04 |  | 0.46 | 0.01 | 0.84 | 0.29 |  | 0.39 | 0.31 |  |
| Uniform Delay, d1 |  | 21.9 | 21.5 |  | 22.7 | 21.4 | 25.6 | 4.4 |  | 27.1 | 5.8 |  |
| Progression Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 |  | 0.5 | 0.1 |  | 1.9 | 0.0 | 37.0 | 0.1 |  | 7.8 | 0.2 |  |
| Delay (s) |  | 22.4 | 21.5 |  | 24.6 | 21.4 | 62.6 | 4.5 |  | 34.9 | 6.0 |  |
| Level of Service |  | C | C |  | C | C | E | A |  | C | A |  |
| Approach Delay (s) |  | 21.8 |  |  | 24.1 |  |  | 18.3 |  |  | 7.0 |  |
| Approach LOS |  | C |  |  | C |  |  | B |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 15.3 |  | HCM Le | vel of S | ervice |  | B |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.36 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 55.8 |  | Sum of lost time (s) |  |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 39.8\% | ICU Level of Service |  |  |  |  | A |  |  |  |
| Analysis Period (min) |  | 15 |  |  |  |  |  |  |  |  |  |  |

C Critical Lane Group

SimTraffic Post-Processor
Trinity County
Average Results from 10 Runs 2009 Conditions (with East Connector)

Summer PM Peak
Queue Length
Signalized

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 150 | 28 | 4 | 59 | 4 | 73 | 7 | 0 | 0 |
|  | Through | 278 | 68 | 7 | 135 | 21 | 172 | 34 | 8 | 0 |
|  | Right Turn | 50 | 22 | 4 | 62 | 7 | 77 | 2 | 0 | 0 |
| SB | Left Turn | 150 | 13 | 5 | 42 | 25 | 69 | 57 | 0 | 0 |
|  | Through | 233 | 61 | 6 | 133 | 21 | 179 | 47 | 7 | 0 |
|  | Right Turn | 50 | 14 | 4 | 52 | 12 | 77 | 5 | 0 | 0 |
| EB | Left Turn | 494 | 52 | 4 | 90 | 10 | 113 | 21 | 8 | 0 |
|  | Through | 494 | 52 | 4 | 90 | 10 | 113 | 21 | 8 | 0 |
|  | Right Turn | 50 | 19 | 4 | 51 | 10 | 68 | 15 | 0 | 0 |
| WB | Left Turn | 328 | 36 | 4 | 69 | 11 | 85 | 20 | 3 | 0 |
|  | Through | 328 | 36 | 4 | 69 | 11 | 85 | 20 | 3 | 0 |
|  | Right Turn | 50 | 7 | 3 | 28 | 7 | 36 | 12 | 0 | 0 |

Intersection 2 SR 299/Washington St
Signalized

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 100 | 26 | 3 | 58 | 4 | 80 | 24 | 0 | 0 |
|  | Through | 590 | 57 | 6 | 131 | 14 | 180 | 29 | 2 | 0 |
|  | Right Turn | 100 | 5 | 2 | 25 | 13 | 49 | 41 | 0 | 0 |
| SB | Left Turn | 100 | 22 | 5 | 52 | 9 | 71 | 30 | 0 | 0 |
|  | Through | 637 | 63 | 7 | 132 | 14 | 168 | 20 | 2 | 0 |
|  | Right Turn | 637 | 63 | 7 | 132 | 14 | 168 | 20 | 2 | 0 |
| EB | Left Turn | 214 | 30 | 4 | 54 | 7 | 63 | 11 | 0 | 0 |
|  | Through | 214 | 30 | 4 | 54 | 7 | 63 | 11 | 0 | 0 |
|  | Right Turn | 214 | 30 | 4 | 54 | 7 | 63 | 11 | 0 | 0 |
| WB | Left Turn | 300 | 25 | 4 | 55 | 9 | 73 | 14 | 0 | 0 |
|  | Through | 300 | 25 | 4 | 55 | 9 | 73 | 14 | 0 | 0 |
|  | Right Turn | 300 | 25 | 4 | 55 | 9 | 73 | 14 | 0 | 0 |


| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn |  |  |  |  |  |  |  |  |  |
|  | Through | 502 | 71 | 11 | 147 | 25 | 201 | 45 | 0 | 0 |
|  | Right Turn | 502 | 71 | 11 | 147 | 25 | 201 | 45 | 0 | 0 |
| SB | Left Turn | 75 | 40 | 3 | 73 | 5 | 85 | 12 | 1 | 0 |
|  | Through | 456 | 30 | 6 | 73 | 12 | 97 | 26 | 0 | 0 |
|  | Right Turn |  |  |  |  |  |  |  |  |  |
| EB | Left Turn |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |
| WB | Left Turn | 1,089 | 35 | 3 | 63 | 6 | 80 | 13 | 0 | 0 |
|  | Through |  |  |  |  |  |  |  |  |  |
|  | Right Turn | 180 | 32 | 3 | 56 | 4 | 70 | 10 | 0 | 0 |

Intersection 4
SR 299/Forest St
Signalized

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 50 | 35 | 4 | 67 | 7 | 76 | 2 | 4 | 0 |
|  | Through | 192 | 28 | 4 | 78 | 15 | 124 | 44 | 1 | 0 |
|  | Right Turn | 192 | 28 | 4 | 78 | 15 | 124 | 44 | 1 | 0 |
| SB | Left Turn | 150 | 10 | 2 | 34 | 6 | 40 | 11 | 0 | 0 |
|  | Through | 1,805 | 52 | 4 | 111 | 8 | 149 | 27 | 0 | 0 |
|  | Right Turn | 1,805 | 52 | 4 | 111 | 8 | 149 | 27 | 0 | 0 |
| EB | Left Turn | 75 | 15 | 2 | 40 | 4 | 46 | 10 | 0 | 0 |
|  | Through | 75 | 15 | 2 | 40 | 4 | 46 | 10 | 0 | 0 |
|  | Right Turn | 393 | 22 | 2 | 45 | 3 | 54 | 10 | 0 | 0 |
| WB | Left Turn | 621 | 30 | 4 | 62 | 6 | 77 | 16 | 2 | 0 |
|  | Through | 621 | 30 | 4 | 62 | 6 | 77 | 16 | 2 | 0 |
|  | Right Turn | 50 | 9 | 2 | 33 | 6 | 45 | 22 | 0 | 0 |

SimTraffic Post-Processor
Trinity County
Average Results from 10 Runs 2040 Conditions (with East Connector)
Queue Length

## Summer PM Peak

Intersection 1
SR 299/Glen Rd
Signalized

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 150 | 29 | 5 | 68 | 16 | 102 | 48 | 0 | 0 |
|  | Through | 278 | 92 | 10 | 181 | 20 | 231 | 52 | 12 | 0 |
|  | Right Turn | 50 | 31 | 5 | 73 | 6 | 78 | 1 | 0 | 0 |
| SB | Left Turn | 150 | 19 | 4 | 51 | 16 | 84 | 49 | 0 | 0 |
|  | Through | 1,315 | 75 | 15 | 155 | 35 | 204 | 70 | 9 | 0 |
|  | Right Turn | 50 | 15 | 3 | 56 | 7 | 78 | 1 | 0 | 0 |
| EB | Left Turn | 494 | 58 | 7 | 100 | 13 | 129 | 29 | 11 | 0 |
|  | Through | 494 | 58 | 7 | 100 | 13 | 129 | 29 | 11 | 0 |
|  | Right Turn | 50 | 20 | 3 | 57 | 8 | 74 | 8 | 0 | 0 |
| WB | Left Turn | 328 | 40 | 5 | 75 | 10 | 95 | 16 | 5 | 0 |
|  | Through | 328 | 40 | 5 | 75 | 10 | 95 | 16 | 5 | 0 |
|  | Right Turn | 50 | 14 | 3 | 42 | 5 | 53 | 19 | 0 | 0 |

Intersection 2
SR 299/Washington St
Signalized

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 100 | 36 | 6 | 76 | 14 | 102 | 31 | 0 | 0 |
|  | Through | 590 | 90 | 11 | 202 | 34 | 289 | 70 | 4 | 0 |
|  | Right Turn | 100 | 34 | 7 | 95 | 17 | 130 | 12 | 0 | 0 |
| SB | Left Turn | 100 | 24 | 5 | 61 | 14 | 92 | 32 | 0 | 0 |
|  | Through | 637 | 92 | 8 | 185 | 25 | 257 | 47 | 5 | 0 |
|  | Right Turn | 637 | 92 | 8 | 185 | 25 | 257 | 47 | 5 | 0 |
| EB | Left Turn | 214 | 29 | 5 | 58 | 8 | 68 | 14 | 0 | 0 |
|  | Through | 214 | 29 | 5 | 58 | 8 | 68 | 14 | 0 | 0 |
|  | Right Turn | 214 | 29 | 5 | 58 | 8 | 68 | 14 | 0 | 0 |
| WB | Left Turn | 300 | 51 | 5 | 92 | 10 | 120 | 23 | 0 | 0 |
|  | Through | 300 | 51 | 5 | 92 | 10 | 120 | 23 | 0 | 0 |
|  | Right Turn | 300 | 51 | 5 | 92 | 10 | 120 | 23 | 0 | 0 |


| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn |  |  |  |  |  |  |  |  |  |
|  | Through | 502 | 77 | 7 | 152 | 15 | 208 | 35 | 0 | 0 |
|  | Right Turn | 502 | 77 | 7 | 152 | 15 | 208 | 35 | 0 | 0 |
| SB | Left Turn | 75 | 49 | 5 | 86 | 8 | 99 | 12 | 2 | 0 |
|  | Through | 456 | 42 | 5 | 94 | 14 | 138 | 29 | 1 | 0 |
|  | Right Turn |  |  |  |  |  |  |  |  |  |
| EB | Left Turn |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |
| WB | Left Turn | 1,089 | 40 | 2 | 75 | 9 | 93 | 27 | 0 | 0 |
|  | Through |  |  |  |  |  |  |  |  |  |
|  | Right Turn | 180 | 38 | 3 | 61 | 5 | 70 | 8 | 0 | 0 |

Intersection 4
SR 299/Forest Ave
Signalized

| Direction | Movement | Storage (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 50 | 41 | 5 | 74 | 7 | 78 | 2 | 6 | 0 |
|  | Through | 192 | 39 | 12 | 94 | 23 | 139 | 38 | 2 | 0 |
|  | Right Turn | 192 | 39 | 12 | 94 | 23 | 139 | 38 | 2 | 0 |
| SB | Left Turn | 150 | 8 | 2 | 30 | 4 | 33 | 0 | 0 | 0 |
|  | Through | 1,805 | 66 | 9 | 132 | 25 | 172 | 65 | 1 | 0 |
|  | Right Turn | 1,805 | 66 | 9 | 132 | 25 | 172 | 65 | 1 | 0 |
| EB | Left Turn | 75 | 18 | 3 | 45 | 3 | 53 | 11 | 0 | 0 |
|  | Through | 75 | 18 | 3 | 45 | 3 | 53 | 11 | 0 | 0 |
|  | Right Turn | 393 | 25 | 1 | 46 | 4 | 62 | 8 | 0 | 0 |
| WB | Left Turn | 621 | 34 | 6 | 65 | 7 | 80 | 17 | 3 | 0 |
|  | Through | 621 | 34 | 6 | 65 | 7 | 80 | 17 | 3 | 0 |
|  | Right Turn | 50 | 7 | 2 | 27 | 5 | 35 | 14 | 0 | 0 |

Arterial Level of Service: NB SR 299

| Cross Street | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Martin Road | 4.2 | 62.2 | 0.5 | 28 |
| East Connector Road | 1.6 | 16.4 | 0.1 | 26 |
|  | 6.8 | 13.7 | 0.1 | 18 |
| Mountain View Street | 1.4 | 9.0 | 0.1 | 24 |
| Levee Road | 2.4 | 28.2 | 0.2 | 28 |
| Weaver Street | 1.0 | 9.3 | 0.1 | 26 |
| Washington Street | 0.6 | 4.9 | 0.0 | 26 |
| Mill Street | 5.5 | 20.6 | 0.1 | 22 |
|  | 2.2 | 18.1 | 0.1 | 26 |
| Lorenz Street | 0.8 | 8.1 | 0.1 | 27 |
| SR 3 | 1.6 | 15.8 | 0.1 | 28 |
| Court Street | 7.1 | 20.2 | 0.1 | 19 |
| Garden Gulch | 2.0 | 14.0 | 0.1 | 25 |
| Total | 3.4 | 9.2 | 0.0 | 19 |

Arterial Level of Service: SB SR 299

| Cross Street | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Forest Ave | 7.3 | 49.5 | 0.3 | 26 |
| Court Street | 1.4 | 7.5 | 0.0 | 23 |
| SR 3 | 3.1 | 14.3 | 0.1 | 25 |
| Lorenz Street | 1.3 | 14.0 | 0.1 | 27 |
| Mill Street | 1.1 | 16.6 | 0.1 | 27 |
| Weaver Street | 0.9 | 8.0 | 0.1 | 28 |
| Masonic Lane | 5.7 | 21.4 | 0.1 | 22 |
| Mountain View Street | 2.1 | 17.0 | 0.1 | 27 |
|  | 0.8 | 5.3 | 0.0 | 24 |
| Glen Road | 0.8 | 9.1 | 0.1 | 27 |
|  | 2.7 | 29.4 | 0.2 | 27 |
| Nugget Lane | 7.0 | 13.9 | 0.1 | 16 |
| Total | 1.6 | 10.2 | 0.1 | 24 |
|  | 1.2 | 14.2 | 0.1 | 30 |

Arterial Level of Service: NB SR 299

| Cross Street | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Martin Road | 4.9 | 63.1 | 0.5 | 27 |
| East Connector Road | 1.9 | 16.6 | 0.1 | 26 |
|  | 8.1 | 15.3 | 0.1 | 16 |
| Mountain View Street | 1.5 | 9.2 | 0.1 | 24 |
| Levee Road | 2.8 | 28.4 | 0.2 | 28 |
| Weaver Street | 1.3 | 9.7 | 0.1 | 25 |
| Washington Street | 0.9 | 5.1 | 0.0 | 26 |
| Mill Street | 7.0 | 22.1 | 0.1 | 21 |
|  | 2.3 | 18.3 | 0.1 | 26 |
| Lorenz Street | 0.8 | 8.2 | 0.1 | 27 |
| SR 3 | 1.7 | 15.8 | 0.1 | 29 |
| Court Street | 8.2 | 21.2 | 0.1 | 18 |
| Garden Gulch | 2.3 | 14.3 | 0.1 | 25 |
| Total | 4.3 | 10.2 | 0.0 | 17 |

Arterial Level of Service: SB SR 299

| Cross Street | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Forest Ave | 8.1 | 50.2 | 0.3 | 25 |
| Court Street | 1.6 | 7.7 | 0.0 | 23 |
| SR 3 | 3.7 | 14.9 | 0.1 | 24 |
| Lorenz Street | 1.5 | 14.4 | 0.1 | 27 |
| Mill Street | 1.3 | 16.9 | 0.1 | 27 |
| Weaver Street | 1.0 | 8.2 | 0.1 | 27 |
| Masonic Lane | 8.1 | 23.8 | 0.1 | 20 |
| Mountain View Street | 2.5 | 17.3 | 0.1 | 26 |
|  | 1.1 | 5.6 | 0.0 | 24 |
| Glen Road | 0.9 | 9.1 | 0.1 | 27 |
|  | 3.2 | 29.9 | 0.2 | 26 |
| Nugget Lane | 6.4 | 13.1 | 0.1 | 17 |
| Total | 1.7 | 10.2 | 0.1 | 23 |

## 1: Glen Road \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 1081 |
| CO Emissions (kg) | 1.01 |
| NOx Emissions (kg) | 0.20 |
| VOC Emissions (kg) | 0.23 |

2: Washington Street \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 901 |
| CO Emissions $(\mathrm{kg})$ | 0.56 |
| NOx Emissions (kg) | 0.11 |
| VOC Emissions $(\mathrm{kg})$ | 0.13 |

3: SR 3 \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 740 |
| CO Emissions (kg) | 0.50 |
| NOX Emissions $(\mathrm{kg})$ | 0.10 |
| VOC Emissions $(\mathrm{kg})$ | 0.12 |

4: Forest Ave \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 690 |
| CO Emissions $(\mathrm{kg})$ | 0.58 |
| NOx Emissions $(\mathrm{kg})$ | 0.11 |
| VOC Emissions $(\mathrm{kg})$ | 0.13 |

## 1: Glen Road \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 1210 |
| CO Emissions (kg) | 1.14 |
| NOx Emissions (kg) | 0.22 |
| VOC Emissions (kg) | 0.27 |

2: Washington Street \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 1171 |
| CO Emissions $(\mathrm{kg})$ | 0.88 |
| NOx Emissions (kg) | 0.17 |
| VOC Emissions $(\mathrm{kg})$ | 0.20 |

3: SR 3 \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 880 |
| CO Emissions $(\mathrm{kg})$ | 0.65 |
| NOX Emissions $(\mathrm{kg})$ | 0.13 |
| VOC Emissions $(\mathrm{kg})$ | 0.15 |

4: Forest Ave \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 832 |
| CO Emissions $(\mathrm{kg})$ | 0.70 |
| NOx Emissions $(\mathrm{kg})$ | 0.14 |
| VOC Emissions $(\mathrm{kg})$ | 0.16 |

## ATTACHMENT D

## SCENARIO 3: SIGNALIZED AND ROUNDABOUT INTERSECTIONS

Trinity County - 2009 Conditions (with East Connector) PM Peak
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Turn | Demand Flow veh/h | $\begin{gathered} \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: SR 299 NB |  |  |  |  |  |  |  |  |  |  |  |
| 3L | L | 47 | 2.0 | 0.506 | 14.0 | LOS B | 4.9 | 123.8 | 0.57 | 0.81 | 29.6 |
| 8T | T | 376 | 2.0 | 0.507 | 7.1 | LOS A | 4.9 | 123.8 | 0.57 | 0.58 | 31.5 |
| 8R | R | 82 | 2.0 | 0.508 | 8.5 | LOS A | 4.9 | 123.8 | 0.57 | 0.64 | 31.4 |
| Approach |  | 506 | 2.0 | 0.507 | 8.0 | LOS B | 4.9 | 123.8 | 0.57 | 0.61 | 31.3 |
| East: East Connector Road WB |  |  |  |  |  |  |  |  |  |  |  |
| 1L | L | 71 | 2.0 | 0.165 | 16.5 | LOS B | 1.1 | 28.7 | 0.67 | 0.84 | 27.8 |
| 6 T | T | 24 | 2.0 | 0.165 | 9.6 | LOS A | 1.1 | 28.7 | 0.67 | 0.71 | 30.4 |
| 6 R | R | 12 | 2.0 | 0.166 | 10.9 | LOS B | 1.1 | 28.7 | 0.67 | 0.75 | 30.1 |
| Approach |  | 106 | 2.0 | 0.165 | 14.3 | LOS B | 1.1 | 28.7 | 0.67 | 0.80 | 28.5 |
| North: SR 299 SB |  |  |  |  |  |  |  |  |  |  |  |
| 7L | L | 24 | 2.0 | 0.444 | 13.5 | LOS B | 4.0 | 102.6 | 0.48 | 0.81 | 29.8 |
| 4 T | T | 365 | 2.0 | 0.446 | 6.7 | LOS A | 4.0 | 102.6 | 0.48 | 0.53 | 32.0 |
| 4R | R | 82 | 2.0 | 0.448 | 8.0 | LOS A | 4.0 | 102.6 | 0.48 | 0.60 | 31.7 |
| Approach |  | 471 | 2.0 | 0.447 | 7.2 | LOS B | 4.0 | 102.6 | 0.48 | 0.55 | 31.8 |
| West: Glen Road EB |  |  |  |  |  |  |  |  |  |  |  |
| 5L | L | 118 | 2.0 | 0.267 | 16.0 | LOS B | 1.9 | 48.4 | 0.66 | 0.85 | 28.0 |
| 2T | T | 35 | 2.0 | 0.267 | 9.2 | LOS A | 1.9 | 48.4 | 0.66 | 0.71 | 30.5 |
| 2R | R | 35 | 2.0 | 0.267 | 10.5 | LOS B | 1.9 | 48.4 | 0.66 | 0.75 | 30.4 |
| Approach |  | 188 | 2.0 | 0.267 | 13.7 | LOS B | 1.9 | 48.4 | 0.66 | 0.80 | 28.8 |
| All Vehic |  | 1271 | 2.0 | 0.507 | 9.1 | LOS A | 4.9 | 123.8 | 0.56 | 0.63 | 30.8 |

Level of Service (Aver. Int. Delay): LOS A. Based on average delay for all vehicle movements. LOS Method: Delay (HCM).
Level of Service (Worst Movement): LOS B. LOS Method for individual vehicle movements: Delay (HCM).
Approach LOS values are based on the worst delay for any vehicle movement.
Roundabout LOS Method: Same as Signalised Intersections.
Roundabout Capacity Model: SIDRA Standard.



c Critical Lane Group

Trinity County - 2009 Conditions (with East Connector) PM Peak
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Turn | Demand Flow veh/h | $\begin{gathered} \text { HV } \\ \% \end{gathered}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \mathrm{v} / \mathrm{c} \\ & \hline \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: SR 299 NB |  |  |  |  |  |  |  |  |  |  |  |
| 3L | L | 89 | 2.0 | 0.265 | 12.5 | LOS B | 2.1 | 52.3 | 0.19 | 0.83 | 29.9 |
| 8T | T | 211 | 2.0 | 0.266 | 5.2 | LOS A | 2.1 | 52.3 | 0.19 | 0.38 | 33.8 |
| 8R | R | 44 | 2.0 | 0.266 | 6.7 | LOS A | 2.1 | 52.3 | 0.19 | 0.50 | 32.9 |
| Approac |  | 344 | 2.0 | 0.266 | 7.3 | LOS B | 2.1 | 52.3 | 0.19 | 0.51 | 32.5 |
| East: Garden Gulch St WB |  |  |  |  |  |  |  |  |  |  |  |
| 1L | L | 48 | 2.0 | 0.084 | 14.3 | LOS B | 0.5 | 13.2 | 0.48 | 0.75 | 29.0 |
| 6 T | T | 12 | 2.0 | 0.084 | 7.1 | LOS A | 0.5 | 13.2 | 0.48 | 0.52 | 31.6 |
| 6 R | R | 12 | 2.0 | 0.084 | 8.5 | LOS A | 0.5 | 13.2 | 0.48 | 0.59 | 31.3 |
| Approac |  | 71 | 2.0 | 0.084 | 12.2 | LOS B | 0.5 | 13.2 | 0.48 | 0.68 | 29.7 |
| North: SR 299 SB |  |  |  |  |  |  |  |  |  |  |  |
| 7L | L | 14 | 2.0 | 0.322 | 13.4 | LOS B | 2.5 | 62.5 | 0.41 | 0.86 | 29.9 |
| 4 T | T | 311 | 2.0 | 0.324 | 6.2 | LOS A | 2.5 | 62.5 | 0.41 | 0.50 | 32.6 |
| 4R | R | 14 | 2.0 | 0.322 | 7.6 | LOS A | 2.5 | 62.5 | 0.41 | 0.59 | 32.2 |
| Approac |  | 338 | 2.0 | 0.324 | 6.5 | LOS B | 2.5 | 62.5 | 0.41 | 0.52 | 32.5 |
| West: Forest Ave EB |  |  |  |  |  |  |  |  |  |  |  |
| 5L | L | 12 | 2.0 | 0.107 | 14.8 | LOS B | 0.7 | 17.6 | 0.54 | 0.81 | 28.9 |
| 2T | T | 12 | 2.0 | 0.107 | 7.6 | LOS A | 0.7 | 17.6 | 0.54 | 0.58 | 31.5 |
| 2R | R | 60 | 2.0 | 0.107 | 9.0 | LOS A | 0.7 | 17.6 | 0.54 | 0.64 | 31.3 |
| Approach |  | 84 | 2.0 | 0.107 | 9.6 | LOS B | 0.7 | 17.6 | 0.54 | 0.66 | 30.9 |
| All Vehic |  | 838 | 2.0 | 0.324 | 7.6 | LOS A | 2.5 | 62.5 | 0.34 | 0.54 | 32.1 |

Level of Service (Aver. Int. Delay): LOS A. Based on average delay for all vehicle movements. LOS Method: Delay (HCM). Level of Service (Worst Movement): LOS B. LOS Method for individual vehicle movements: Delay (HCM).
Approach LOS values are based on the worst delay for any vehicle movement.
Roundabout LOS Method: Same as Signalised Intersections.
Roundabout Capacity Model: SIDRA Standard.


Trinity County - 2040 Conditions (with East Connector) PM Peak
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Turn | Demand Flow veh/h | $\begin{aligned} & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance <br> ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: SR 299 NB |  |  |  |  |  |  |  |  |  |  |  |
| 3L | L | 47 | 2.0 | 0.581 | 14.3 | LOS B | 6.1 | 154.1 | 0.64 | 0.80 | 29.5 |
| 8T | T | 424 | 2.0 | 0.583 | 7.4 | LOS A | 6.1 | 154.1 | 0.64 | 0.61 | 31.1 |
| 8R | R | 106 | 2.0 | 0.582 | 8.8 | LOS A | 6.1 | 154.1 | 0.64 | 0.66 | 31.1 |
| Approach |  | 576 | 2.0 | 0.582 | 8.2 | LOS B | 6.1 | 154.1 | 0.64 | 0.64 | 31.0 |
| East: East Connector Road WB |  |  |  |  |  |  |  |  |  |  |  |
| 1L | L | 94 | 2.0 | 0.234 | 17.1 | LOS B | 1.7 | 42.7 | 0.72 | 0.88 | 27.4 |
| 6 T | T | 24 | 2.0 | 0.233 | 10.3 | LOS B | 1.7 | 42.7 | 0.72 | 0.77 | 29.9 |
| 6 R | R | 24 | 2.0 | 0.233 | 11.6 | LOS B | 1.7 | 42.7 | 0.72 | 0.80 | 29.6 |
| Approach |  | 141 | 2.0 | 0.234 | 15.1 | LOS B | 1.7 | 42.7 | 0.72 | 0.85 | 28.1 |
| North: SR 299 SB |  |  |  |  |  |  |  |  |  |  |  |
| 7L | L | 35 | 2.0 | 0.504 | 13.9 | LOS B | 4.9 | 124.2 | 0.55 | 0.81 | 29.7 |
| 4 T | T | 412 | 2.0 | 0.508 | 7.0 | LOS A | 4.9 | 124.2 | 0.55 | 0.57 | 31.6 |
| 4R | R | 71 | 2.0 | 0.508 | 8.3 | LOS A | 4.9 | 124.2 | 0.55 | 0.63 | 31.5 |
| Approach |  | 518 | 2.0 | 0.507 | 7.7 | LOS B | 4.9 | 124.2 | 0.55 | 0.59 | 31.5 |
| West: Glen Road EB |  |  |  |  |  |  |  |  |  |  |  |
| 5L | L | 118 | 2.0 | 0.293 | 16.9 | LOS B | 2.1 | 54.3 | 0.72 | 0.88 | 27.6 |
| 2T | T | 35 | 2.0 | 0.294 | 10.0 | LOS B | 2.1 | 54.3 | 0.72 | 0.77 | 30.1 |
| 2R | R | 35 | 2.0 | 0.294 | 11.4 | LOS B | 2.1 | 54.3 | 0.72 | 0.80 | 29.8 |
| Approach |  | 188 | 2.0 | 0.293 | 14.6 | LOS B | 2.1 | 54.3 | 0.72 | 0.85 | 28.4 |
| All Vehic |  | 1424 | 2.0 | 0.582 | 9.5 | LOS A | 6.1 | 154.1 | 0.63 | 0.67 | 30.5 |

Level of Service (Aver. Int. Delay): LOS A. Based on average delay for all vehicle movements. LOS Method: Delay (HCM).
Level of Service (Worst Movement): LOS B. LOS Method for individual vehicle movements: Delay (HCM).
Approach LOS values are based on the worst delay for any vehicle movement.
Roundabout LOS Method: Same as Signalised Intersections.
Roundabout Capacity Model: SIDRA Standard.


|  | 4 | $\rightarrow$ | $\checkmark$ | 4 |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | \& |  | ${ }^{7}$ | 4 | 「 | ${ }^{*}$ | $\uparrow$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Frt |  | 0.91 |  |  | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 |  |
| Flt Protected |  | 0.99 |  |  | 0.96 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  |
| Satd. Flow (prot) |  | 1682 |  |  | 1768 |  | 1770 | 1863 | 1583 | 1770 | 1850 |  |
| Flt Permitted |  | 0.94 |  |  | 0.78 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  |
| Satd. Flow (perm) |  | 1596 |  |  | 1442 |  | 1770 | 1863 | 1583 | 1770 | 1850 |  |
| Volume (vph) | 10 | 10 | 40 | 90 | 10 | 10 | 50 | 380 | 110 | 30 | 410 | 20 |
| Peak-hour factor, PHF | 0.73 | 0.73 | 0.73 | 0.70 | 0.70 | 0.70 | 0.87 | 0.87 | 0.87 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 14 | 14 | 55 | 129 | 14 | 14 | 57 | 437 | 126 | 33 | 456 | 22 |
| RTOR Reduction (vph) | 0 | 43 | 0 | 0 | 5 | 0 | 0 | 0 | 59 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 0 | 40 | 0 | 0 | 152 | 0 | 57 | 437 | 67 | 33 | 476 | 0 |
| Turn Type | Perm |  |  | Perm |  |  | Prot |  | Perm | Prot |  |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  |  |  | 2 |  |  |  |
| Actuated Green, G (s) |  | 11.6 |  |  | 11.6 |  | 3.0 | 27.1 | 27.1 | 2.6 | 26.7 |  |
| Effective Green, g (s) |  | 11.6 |  |  | 11.6 |  | 3.0 | 27.1 | 27.1 | 2.6 | 26.7 |  |
| Actuated g/C Ratio |  | 0.22 |  |  | 0.22 |  | 0.06 | 0.51 | 0.51 | 0.05 | 0.50 |  |
| Clearance Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) |  | 347 |  |  | 314 |  | 100 | 947 | 805 | 86 | 927 |  |
| v/s Ratio Prot |  |  |  |  |  |  | c0.03 | 0.23 |  | 0.02 | c0.26 |  |
| v/s Ratio Perm |  | 0.03 |  |  | c0.11 |  |  |  | 0.04 |  |  |  |
| v/c Ratio |  | 0.12 |  |  | 0.48 |  | 0.57 | 0.46 | 0.08 | 0.38 | 0.51 |  |
| Uniform Delay, d1 |  | 16.7 |  |  | 18.2 |  | 24.5 | 8.4 | 6.7 | 24.6 | 8.9 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Incremental Delay, d2 |  | 0.1 |  |  | 1.2 |  | 7.3 | 0.4 | 0.0 | 2.8 | 0.5 |  |
| Delay (s) |  | 16.9 |  |  | 19.4 |  | 31.8 | 8.8 | 6.8 | 27.4 | 9.4 |  |
| Level of Service |  | B |  |  | B |  | C | A | A | C | A |  |
| Approach Delay (s) |  | 16.9 |  |  | 19.4 |  |  | 10.5 |  |  | 10.6 |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 11.9 |  | HCM Lev | el of S | ervice |  | B |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.51 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 53.3 |  | Sum of lo | st time |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 48.9\% |  | CU Leve | of Servir | vice |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |


c Critical Lane Group

Trinity County - 2040 Conditions (with East Connector) PM Peak
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Turn | Demand Flow veh/h | $\begin{gathered} \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: SR 299 NB |  |  |  |  |  |  |  |  |  |  |  |
| 3L | L | 100 | 2.0 | 0.332 | 12.6 | LOS B | 2.8 | 71.4 | 0.24 | 0.81 | 29.9 |
| 8T | T | 267 | 2.0 | 0.332 | 5.3 | LOS A | 2.8 | 71.4 | 0.24 | 0.39 | 33.5 |
| 8R | R | 56 | 2.0 | 0.333 | 6.8 | LOS A | 2.8 | 71.4 | 0.24 | 0.51 | 32.7 |
| Approac |  | 422 | 2.0 | 0.332 | 7.2 | LOS B | 2.8 | 71.4 | 0.24 | 0.51 | 32.4 |
| East: Garden Gulch St WB |  |  |  |  |  |  |  |  |  |  |  |
| 1L | L | 60 | 2.0 | 0.106 | 15.0 | LOS B | 0.7 | 17.1 | 0.54 | 0.77 | 28.6 |
| 6 T | T | 12 | 2.0 | 0.106 | 7.7 | LOS A | 0.7 | 17.1 | 0.54 | 0.57 | 31.2 |
| 6 R | R | 12 | 2.0 | 0.106 | 9.2 | LOS A | 0.7 | 17.1 | 0.54 | 0.64 | 31.0 |
| Approac |  | 83 | 2.0 | 0.106 | 13.1 | LOS B | 0.7 | 17.1 | 0.54 | 0.72 | 29.2 |
| North: SR 299 SB |  |  |  |  |  |  |  |  |  |  |  |
| 7L | L | 14 | 2.0 | 0.386 | 13.7 | LOS B | 3.1 | 78.6 | 0.47 | 0.86 | 29.8 |
| 4 T | T | 365 | 2.0 | 0.385 | 6.5 | LOS A | 3.1 | 78.6 | 0.47 | 0.53 | 32.3 |
| 4R | R | 14 | 2.0 | 0.386 | 7.9 | LOS A | 3.1 | 78.6 | 0.47 | 0.62 | 32.0 |
| Approac |  | 392 | 2.0 | 0.385 | 6.8 | LOS B | 3.1 | 78.6 | 0.47 | 0.55 | 32.2 |
| West: Forest Ave EB |  |  |  |  |  |  |  |  |  |  |  |
| 5L | L | 24 | 2.0 | 0.147 | 15.4 | LOS B | 1.0 | 25.1 | 0.60 | 0.83 | 28.5 |
| 2 T | T | 12 | 2.0 | 0.147 | 8.2 | LOS A | 1.0 | 25.1 | 0.60 | 0.63 | 31.1 |
| 2R | R | 72 | 2.0 | 0.147 | 9.6 | LOS A | 1.0 | 25.1 | 0.60 | 0.69 | 31.0 |
| Approach |  | 108 | 2.0 | 0.147 | 10.8 | LOS B | 1.0 | 25.1 | 0.60 | 0.71 | 30.4 |
| All Vehicles |  | 1006 | 2.0 | 0.385 | 7.9 | LOS A | 3.1 | 78.6 | 0.39 | 0.56 | 31.8 |

Level of Service (Aver. Int. Delay): LOS A. Based on average delay for all vehicle movements. LOS Method: Delay (HCM). Level of Service (Worst Movement): LOS B. LOS Method for individual vehicle movements: Delay (HCM).
Approach LOS values are based on the worst delay for any vehicle movement.
Roundabout LOS Method: Same as Signalised Intersections.
Roundabout Capacity Model: SIDRA Standard.


SimTraffic Post-Processor
Average Results from 10 Runs Queue Length

Trinity County

## 2009 Conditions (with East Connector)

Summer PM Peak

Intersection 1 SR 299/Glen Road
Unsignalized

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 188 | 51 | 5 | 100 | 10 | 118 | 18 | 0 | 0 |
|  | Through | 188 | 51 | 5 | 100 | 10 | 118 | 18 | 0 | 0 |
|  | Right Turn | 188 | 51 | 5 | 100 | 10 | 118 | 18 | 0 | 0 |
| SB | Left Turn | 159 | 43 | 10 | 90 | 19 | 128 | 52 | 0 | 0 |
|  | Through | 159 | 43 | 10 | 90 | 19 | 128 | 52 | 0 | 0 |
|  | Right Turn | 159 | 43 | 10 | 90 | 19 | 128 | 52 | 0 | 0 |
| EB | Left Turn | 403 | 35 | 6 | 67 | 8 | 77 | 11 | 0 | 0 |
|  | Through | 403 | 35 | 6 | 67 | 8 | 77 | 11 | 0 | 0 |
|  | Right Turn | 403 | 35 | 6 | 67 | 8 | 77 | 11 | 0 | 0 |
| WB | Left Turn | 248 | 24 | 3 | 53 | 3 | 62 | 13 | 0 | 0 |
|  | Through | 248 | 24 | 3 | 53 | 3 | 62 | 13 | 0 | 0 |
|  | Right Turn | 248 | 24 | 3 | 53 | 3 | 62 | 13 | 0 | 0 |

Intersection 2
SR 299/Washington Street
Signalized

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 100 | 27 | 4 | 59 | 7 | 78 | 28 | 0 | 0 |
|  | Through | 590 | 54 | 9 | 121 | 17 | 160 | 30 | 1 | 0 |
|  | Right Turn | 100 | 5 | 3 | 30 | 17 | 62 | 42 | 0 | 0 |
| SB | Left Turn | 100 | 25 | 5 | 58 | 11 | 77 | 31 | 0 | 0 |
|  | Through | 637 | 58 | 9 | 130 | 27 | 170 | 54 | 1 | 0 |
|  | Right Turn | 637 | 58 | 9 | 130 | 27 | 170 | 54 | 1 | 0 |
| EB | Left Turn | 214 | 28 | 4 | 56 | 8 | 69 | 15 | 0 | 0 |
|  | Through | 214 | 28 | 4 | 56 | 8 | 69 | 15 | 0 | 0 |
|  | Right Turn | 214 | 28 | 4 | 56 | 8 | 69 | 15 | 0 | 0 |
| WB | Left Turn | 300 | 28 | 3 | 57 | 7 | 76 | 18 | 0 | 0 |
|  | Through | 300 | 28 | 3 | 57 | 7 | 76 | 18 | 0 | 0 |
|  | Right Turn | 300 | 28 | 3 | 57 | 7 | 76 | 18 | 0 | 0 |

Trinity County
Average Results from 10 Runs 2009 Conditions (with East Connector) Summer PM Peak
Intersection 3
SR 299/SR 3
Signalized

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn |  |  |  |  |  |  |  |  |  |
|  | Through | 502 | 67 | 7 | 143 | 18 | 178 | 29 | 0 | 0 |
|  | Right Turn | 502 | 67 | 7 | 143 | 18 | 178 | 29 | 0 | 0 |
| SB | Left Turn | 75 | 39 | 4 | 72 | 9 | 84 | 12 | 1 | 0 |
|  | Through | 456 | 29 | 5 | 73 | 8 | 96 | 18 | 1 | 0 |
|  | Right Turn |  |  |  |  |  |  |  |  |  |
| EB | Left Turn |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |
| WB | Left Turn | 1,089 | 36 | 3 | 66 | 6 | 82 | 13 | 0 | 0 |
|  | Through |  |  |  |  |  |  |  |  |  |
|  | Right Turn | 180 | 32 | 3 | 57 | 7 | 71 | 13 | 0 | 0 |

Intersection 4
SR 299/Forest Avenue
Unsignalized

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 100 | 16 | 4 | 50 | 7 | 62 | 10 | 0 | 0 |
|  | Through | 100 | 16 | 4 | 50 | 7 | 62 | 10 | 0 | 0 |
|  | Right Turn | 100 | 16 | 4 | 50 | 7 | 62 | 10 | 0 | 0 |
| SB | Left Turn | 1,708 | 29 | 5 | 66 | 5 | 79 | 14 | 0 | 0 |
|  | Through | 1,708 | 29 | 5 | 66 | 5 | 79 | 14 | 0 | 0 |
|  | Right Turn | 1,708 | 29 | 5 | 66 | 5 | 79 | 14 | 0 | 0 |
| EB | Left Turn | 301 | 13 | 5 | 40 | 8 | 49 | 12 | 0 | 0 |
|  | Through | 301 | 13 | 5 | 40 | 8 | 49 | 12 | 0 | 0 |
|  | Right Turn | 301 | 13 | 5 | 40 | 8 | 49 | 12 | 0 | 0 |
| WB | Left Turn | 519 | 11 | 4 | 40 | 11 | 56 | 23 | 0 | 0 |
|  | Through | 519 | 11 | 4 | 40 | 11 | 56 | 23 | 0 | 0 |
|  | Right Turn | 519 | 11 | 4 | 40 | 11 | 56 | 23 | 0 | 0 |

SimTraffic Post-Processor
Trinity County
Average Results from 10 Runs 2040 Conditions (with East Connector)

Summer PM Peak
Queue Length
Unsignalized

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 754 | 57 | 5 | 108 | 15 | 143 | 44 | 0 | 0 |
|  | Through | 188 | 57 | 5 | 108 | 15 | 143 | 44 | 0 | 0 |
|  | Right Turn | 188 | 57 | 5 | 108 | 15 | 143 | 44 | 0 | 0 |
| SB | Left Turn | 1,241 | 48 | 5 | 96 | 14 | 136 | 43 | 0 | 0 |
|  | Through | 159 | 48 | 5 | 96 | 14 | 136 | 43 | 0 | 0 |
|  | Right Turn | 159 | 48 | 5 | 96 | 14 | 136 | 43 | 0 | 0 |
| EB | Left Turn | 403 | 35 | 5 | 68 | 11 | 79 | 27 | 0 | 0 |
|  | Through | 403 | 35 | 5 | 68 | 11 | 79 | 27 | 0 | 0 |
|  | Right Turn | 403 | 35 | 5 | 68 | 11 | 79 | 27 | 0 | 0 |
| WB | Left Turn | 248 | 31 | 3 | 63 | 9 | 75 | 25 | 0 | 0 |
|  | Through | 248 | 31 | 3 | 63 | 9 | 75 | 25 | 0 | 0 |
|  | Right Turn | 248 | 31 | 3 | 63 | 9 | 75 | 25 | 0 | 0 |

Intersection 2
SR 299/Washington Street
Signalized

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 100 | 35 | 4 | 70 | 9 | 84 | 29 | 0 | 0 |
|  | Through | 590 | 79 | 14 | 176 | 41 | 248 | 81 | 3 | 0 |
|  | Right Turn | 100 | 28 | 5 | 79 | 14 | 122 | 13 | 0 | 0 |
| SB | Left Turn | 100 | 24 | 4 | 59 | 9 | 85 | 30 | 0 | 0 |
|  | Through | 637 | 88 | 12 | 173 | 30 | 222 | 47 | 4 | 0 |
|  | Right Turn | 637 | 88 | 12 | 173 | 30 | 222 | 47 | 4 | 0 |
| EB | Left Turn | 214 | 29 | 2 | 57 | 5 | 70 | 13 | 0 | 0 |
|  | Through | 214 | 29 | 2 | 57 | 5 | 70 | 13 | 0 | 0 |
|  | Right Turn | 214 | 29 | 2 | 57 | 5 | 70 | 13 | 0 | 0 |
| WB | Left Turn | 300 | 46 | 3 | 81 | 9 | 98 | 22 | 0 | 0 |
|  | Through | 300 | 46 | 3 | 81 | 9 | 98 | 22 | 0 | 0 |
|  | Right Turn | 300 | 46 | 3 | 81 | 9 | 98 | 22 | 0 | 0 |


| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn |  |  |  |  |  |  |  |  |  |
|  | Through | 502 | 79 | 13 | 160 | 25 | 199 | 43 | 0 | 0 |
|  | Right Turn | 502 | 79 | 13 | 160 | 25 | 199 | 43 | 0 | 0 |
| SB | Left Turn | 75 | 48 | 4 | 84 | 7 | 103 | 14 | 2 | 0 |
|  | Through | 456 | 40 | 8 | 91 | 17 | 146 | 36 | 1 | 0 |
|  | Right Turn |  |  |  |  |  |  |  |  |  |
| EB | Left Turn |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |
| WB | Left Turn | 1,089 | 41 | 3 | 76 | 7 | 95 | 11 | 0 | 0 |
|  | Through |  |  |  |  |  |  |  |  |  |
|  | Right Turn | 180 | 38 | 4 | 65 | 8 | 87 | 24 | 0 | 0 |

Intersection 4
SR 299/Forest Ave
Unsignalized

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  | 95th Queue (ft) |  | Maximum Queue (ft) |  | Block Time \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 100 | 23 | 5 | 63 | 9 | 78 | 14 | 0 | 0 |
|  | Through | 100 | 23 | 5 | 63 | 9 | 78 | 14 | 0 | 0 |
|  | Right Turn | 100 | 23 | 5 | 63 | 9 | 78 | 14 | 0 | 0 |
| SB | Left Turn | 1,708 | 35 | 6 | 75 | 8 | 93 | 22 | 0 | 0 |
|  | Through | 1,708 | 35 | 6 | 75 | 8 | 93 | 22 | 0 | 0 |
|  | Right Turn | 1,708 | 35 | 6 | 75 | 8 | 93 | 22 | 0 | 0 |
| EB | Left Turn | 301 | 20 | 2 | 52 | 5 | 68 | 15 | 0 | 0 |
|  | Through | 301 | 20 | 2 | 52 | 5 | 68 | 15 | 0 | 0 |
|  | Right Turn | 301 | 20 | 2 | 52 | 5 | 68 | 15 | 0 | 0 |
| WB | Left Turn | 519 | 16 | 4 | 47 | 7 | 61 | 19 | 0 | 0 |
|  | Through | 519 | 16 | 4 | 47 | 7 | 61 | 19 | 0 | 0 |
|  | Right Turn | 519 | 16 | 4 | 47 | 7 | 61 | 19 | 0 | 0 |

Arterial Level of Service: NB SR 299

| Cross Street | Delay <br> $(\mathrm{s} /$ veh $)$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Martin Road | 4.1 | 62.7 | 0.5 | 28 |
| East Connector Road | 1.7 | 16.5 | 0.1 | 26 |
|  | 5.1 | 10.2 | 0.1 | 25 |
| Mountain View Street | 0.5 | 17.7 | 0.1 | 12 |
| Levee Road | 1.9 | 27.8 | 0.2 | 28 |
| Weaver Street | 0.9 | 9.3 | 0.1 | 26 |
| Washington Street | 0.6 | 4.9 | 0.0 | 27 |
| Mill Street | 5.0 | 20.1 | 0.1 | 23 |
|  | 2.2 | 18.1 | 0.1 | 26 |
| Lorenz Street | 0.8 | 8.2 | 0.1 | 27 |
| SR 3 | 1.6 | 15.9 | 0.1 | 28 |
| Court Street | 6.9 | 20.0 | 0.1 | 19 |
| Garden Gulch | 2.6 | 14.6 | 0.1 | 24 |
| Total | 3.2 | 6.7 | 0.0 | 26 |

Arterial Level of Service: SB SR 299

| Cross Street | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Forest Ave | 5.8 | 45.6 | 0.3 | 28 |
| Court Street | 0.5 | 15.5 | 0.0 | 11 |
| SR 3 | 2.6 | 13.9 | 0.1 | 25 |
| Lorenz Street | 1.2 | 13.9 | 0.1 | 28 |
| Mill Street | 1.1 | 16.7 | 0.1 | 27 |
| Weaver Street | 0.9 | 8.0 | 0.1 | 28 |
| Masonic Lane | 5.1 | 20.7 | 0.1 | 23 |
| Mountain View Street | 2.1 | 17.0 | 0.1 | 27 |
|  | 0.8 | 5.3 | 0.0 | 25 |
| Glen Road | 0.8 | 9.1 | 0.1 | 27 |
|  | 3.0 | 29.6 | 0.2 | 26 |
| Nugget Lane | 4.6 | 9.4 | 0.1 | 23 |
| Total | 0.5 | 19.7 | 0.1 | 12 |

## Arterial Level of Service: NB SR 299

| Cross Street | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Martin Road | 4.7 | 62.9 | 0.5 | 28 |
| East Connector Road | 2.0 | 16.8 | 0.1 | 26 |
|  | 5.7 | 10.8 | 0.1 | 24 |
| Mountain View Street | 0.5 | 17.7 | 0.1 | 12 |
| Levee Road | 2.1 | 27.6 | 0.2 | 28 |
| Weaver Street | 1.1 | 9.5 | 0.1 | 26 |
| Washington Street | 0.8 | 5.0 | 0.0 | 27 |
| Mill Street | 6.9 | 22.0 | 0.1 | 21 |
|  | 2.3 | 18.2 | 0.1 | 26 |
| Lorenz Street | 0.9 | 8.2 | 0.1 | 27 |
| SR 3 | 1.8 | 15.8 | 0.1 | 28 |
| Court Street | 8.2 | 21.2 | 0.1 | 18 |
| Garden Gulch | 2.9 | 14.9 | 0.1 | 24 |
| Total | 3.4 | 6.9 | 0.0 | 26 |

Arterial Level of Service: SB SR 299

| Cross Street | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: |
| Forest Ave | 6.4 | 46.5 | 0.3 | 27 |
| Court Street | 0.7 | 15.3 | 0.0 | 12 |
| SR 3 | 3.2 | 14.5 | 0.1 | 24 |
| Lorenz Street | 1.4 | 14.4 | 0.1 | 27 |
| Mill Street | 1.2 | 16.8 | 0.1 | 27 |
|  | 1.0 | 8.1 | 0.1 | 27 |
| Weaver Street | 7.6 | 23.3 | 0.1 | 20 |
| Masonic Lane | 2.5 | 17.3 | 0.1 | 26 |
| Mountain View Street | 1.0 | 5.4 | 0.0 | 25 |
|  | 0.9 | 9.1 | 0.1 | 27 |
| Glen Road | 3.5 | 30.2 | 0.2 | 26 |
|  | 4.3 | 9.1 | 0.1 | 24 |
| Nugget Lane | 0.6 | 19.8 | 0.1 | 12 |
| Total | 1.0 | 14.7 | 0.1 | 29 |

## 1: Glen Road \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 1080 |
| CO Emissions (kg) | 1.03 |
| NOx Emissions (kg) | 0.20 |
| VOC Emissions (kg) | 0.24 |

2: Washington Street \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 901 |
| CO Emissions $(\mathrm{kg})$ | 0.56 |
| NOx Emissions (kg) | 0.11 |
| VOC Emissions $(\mathrm{kg})$ | 0.13 |

3: SR 3 \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 740 |
| CO Emissions (kg) | 0.50 |
| NOX Emissions $(\mathrm{kg})$ | 0.10 |
| VOC Emissions $(\mathrm{kg})$ | 0.12 |

4: Forest Ave \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 691 |
| CO Emissions $(\mathrm{kg})$ | 0.60 |
| NOx Emissions $(\mathrm{kg})$ | 0.12 |
| VOC Emissions $(\mathrm{kg})$ | 0.14 |

## 1: Glen Road \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 1211 |
| CO Emissions (kg) | 1.15 |
| NOx Emissions (kg) | 0.22 |
| VOC Emissions (kg) | 0.27 |

2: Washington Street \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 1171 |
| CO Emissions (kg) | 0.87 |
| NOx Emissions (kg) | 0.17 |
| VOC Emissions (kg) | 0.20 |

3: SR 3 \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 880 |
| CO Emissions $(\mathrm{kg})$ | 0.65 |
| NOX Emissions $(\mathrm{kg})$ | 0.13 |
| VOC Emissions $(\mathrm{kg})$ | 0.15 |

4: Forest Ave \& SR 299

| Direction | All |
| :--- | ---: |
| Volume (vph) | 832 |
| CO Emissions $(\mathrm{kg})$ | 0.71 |
| NOx Emissions $(\mathrm{kg})$ | 0.14 |
| VOC Emissions $(\mathrm{kg})$ | 0.17 |

## ATTACHMENT E <br> TRAFFIC VIBRATION ASSESSMENT: TRINITY COUNTY INTERSECTION IMPROVEMENTS

## Traffic Vibration Assessment

## Trinity County Intersection Improvements

Weaverville, California (Trinity County)
BAC Job \#2009-028

Prepared For:

## Fehr \& Peers

Attn: Katy Cole
50 West Liberty Street, Suite 1090
Reno, California 89501

Prepared By:

## Bollard Acoustical Consultants, Inc.



Paul Bollard, President

August 1, 2010

BOLLARD
Acoustical Consultants

## INTRODUCTION

Trinity County is considering improvements to three intersections in the town of Weaverville, California. Those intersections are as follows:

- State Route 299 / Washington Street
- State Route 299 / State Route 3
- State Route 299 / Forest Avenue

Currently, there are no controls on State Route 299, with stop signs controlling traffic on the roadways which intersect that route. The improvements being considered consist of signalization of the intersections identified above. The locations of the subject intersections are identified on Figure 1.

Figure 1 - Trinity County Study Intersections


One effect of the intersection signalization would be that heavy trucks passing through Weaverville on SR 299 which currently do not stop would occasionally be required to stop for red lights. Trinity County has expressed concerns that the acceleration and deceleration of heavy trucks on SR 299 at future signalized intersections where trucks are currently not required to stop may result in adverse vibration generation at nearby businesses. In response to these concerns, the acoustic and vibration consulting firm of Bollard Acoustical Consultants, Inc. (BAC) was retained by Fehr \& Peers Associates, Transportation Engineers to conduct a vibration analysis of the intersections in question. This report contains the results of that analysis.

## VIBRATION TERMINOLOGY

Vibration is like noise in that it involves a source, a transmission path, and a receiver. While vibration is related to noise, it differs in that in that noise is generally considered to be pressure waves transmitted through air, whereas vibration usually consists of the excitation of a structure or surface. As with noise, vibration consists of an amplitude and frequency. A person's perception to vibration will depend on their individual sensitivity, as well as the amplitude and frequency of the source and the response of the system which is vibrating.

Vibration can be measured in terms of acceleration, velocity, or displacement. A common practice is to monitor vibration measures in terms of peak particle velocities in inches per second (ppv in/sec). Standards pertaining to perception as well as damage to structures have been developed for vibration levels defined in terms of peak particle velocities.

## CRITERIA FOR ACCEPTABLE VIBRATION EXPOSURE

Human and structural response to different vibration levels is influenced by a number of factors, including ground type, distance between source and receptor, duration of excitation, and the number of perceived vibration events. Table 1, which was developed by Caltrans, shows the vibration levels which would normally be required to result in damage to structures. The vibration levels are presented in terms of peak particle velocity in inches per second. Table 1 indicates that the threshold for damage to structures ranges from 2 to $6 \mathrm{in} / \mathrm{sec}$. One-half this minimum threshold, or $1 \mathrm{in} / \mathrm{sec}$ p.p.v. is considered a safe criterion that would protect against architectural or structural damage. The threshold at which human annoyance could occur is $0.1 \mathrm{in} / \mathrm{sec}$ p.p.v.

| Effects of Various Vibration Levels on People and Buildings |  |  |
| :---: | :---: | :---: |
| Peak Particle Velocity (in/sec) | Human Reaction | Effect on Buildings |
| 0-. 006 | Imperceptible by people | Vibrations unlikely to cause damage of any type |
| .006-.02 | Range of Threshold of perception | Vibrations unlikely to cause damage of any type |
| . 08 | Vibrations clearly perceptible | Recommended upper level of which ruins and ancient monuments should be subjected |
| 0.1 | Level at which continuous vibrations begin to annoy people | Virtually no risk of architectural damage to normal buildings |
| 0.2 | Vibrations annoying to people in buildings | Threshold at which there is a risk of architectural damage to normal dwellings |
| 1.0 |  | Architectural Damage |
| 2.0 |  | Structural Damage to Residential Buildings |
| 6.0 |  | Structural Damage to Commercial Buildings |
| Source: Survey of Earth-borne Vibrations due to Highway Construction and Highway Traffic, Caltrans 1976. |  |  |

## EVALUATION OF TRAFFIC VIBRATION LEVELS

To quantify traffic vibration levels in the City of Weaverville, BAC conducted vibration measurements of several automobile and heavy truck passages at the intersection if SR-299 and SR-3 on the afternoon of Thursday July 15, 2010. BAC also intended to conduct similar measurements at the two other study intersections, but the results of the measurements conducted at the SR-3 / SR-288 intersection rendered those additional measurements unnecessary (additional explanation is provided below). The vibration measurements consisted of peak particle velocity sampling at the edge of roadway, approximately 15 feet from near lane traffic, and 30 feet from far lane traffic.

The measurements were conducted using a Larson-Davis Laboratories Model HVM-100 Vibration Analyzer with a PCB Electronics Model 353B51 ICP Vibration Transducer. The test system is a Type I instrument designed for use in assessing vibration as perceived by human beings, and meets the full requirements of ISO 8041:1990(E). Atmospheric conditions present during the tests were within the operating parameters of the instrument. A photograph of the vibration measurement setup is provided in Figure 2. A summary of the vibration measurement results is provided in Table 2.

Figure 2 - Vibration Monitoring Equipment Setup


| Table 2 <br> Vibration Measurement Results <br> SR-299 / SR-4 Intersection - Weaverville, California July 15, 2010 |  |  |  |
| :---: | :---: | :---: | :---: |
| Vehicle | Operation ${ }^{1}$ | Distance (ft) | Peak Particle Velocity (in./sec.) |
| None - Ambient | n/a | n/a | 0.0069 |
| Auto | c | 15 | 0.0072 |
| Logging Truck | c | 30 | 0.0215 |
| None - Ambient | n/a | n/a | 0.0069 |
| Auto | a | 15 | 0.0078 |
| Logging Truck | a | 15 | 0.0672 |
| Auto | d | 30 | 0.0071 |
| None - Ambient | n/a | n/a | 0.0069 |
| Logging Truck | d | 30 | 0.0226 |
| Logging Truck | d | 30 | 0.0318 |
| Heavy truck | a | 15 | 0.0439 |
| Motorcycle | a | 15 | 0.0082 |
| None - Ambient | n/a | n/a | 0.0069 |
| Heavy Truck | c | 15 | 0.0187 |
| Logging Truck | c | 30 | 0.0122 |
| Fire Engine | a | 15 | 0.0087 |
| Large RV | a | 15 | 0.0087 |
| 1. A = Acceleratin urce: Bollard Acous | celerating, C ultants | Speed |  |

Comparison of the Table 2 data against the Table 1 vibration thresholds indicates that the measured vibration levels were below the thresholds of human perception and well below levels required to result in damage to structures. In addition, there were no appreciable differences in measured vibration levels between heavy trucks accelerating, decelerating, or moving through the study intersection at constant speeds. As a result of the very low vibration levels measured at the intersection of SR-3 \& SR-299, it was determined that additional monitoring of similar vehicles at the two other study intersections in Weaverville were not warranted.

## CONCLUSIONS

Due to the very low levels of vibration measured in close proximity to heavy trucks accelerating, decelerating, and passing the monitoring site at constant speed, this analysis concludes that the introduction of traffic controls at any of the three (3) subject intersections in Weaverville would not result in appreciable changes in vibration levels at existing structures located near those intersections, and that resulting vibration levels would be well below levels required for annoyance to humans or damage to structures.

ATTACHMENT F
CENTER STREET CONVERSION ANALYSIS

|  | 1 |  | $\dagger$ | $p$ |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | \% | F' | $\hat{\beta}$ |  | \% | $\uparrow$ |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Grade | 0\% |  | 0\% |  |  | 0\% |  |
| Volume (veh/h) | 68 | 43 | 214 | 90 | 68 | 201 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.87 | 0.87 | 0.86 | 0.86 |  |
| Hourly flow rate (vph) | 75 | 47 | 246 | 103 | 79 | 234 |  |
| Pedestrians |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |
| Walking Speed (fts) |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type | None |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC , conflicting volume | 690 | 298 |  |  | 349 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu, unblocked vol | 690 | 298 |  |  | 349 |  |  |
| tC , single (s) | 6.4 | 6.2 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 |  |  | 2.2 |  |  |
| p0 queue free \% | 81 | 94 |  |  | 93 |  |  |
| cM capacity (veh/h) | 384 | 742 |  |  | 1209 |  |  |
| Direction, Lane \# | WB 1 | WB 2 | NB 1 | SB 1 | SB 2 |  |  |
| Volume Total | 75 | 47 | 349 | 79 | 234 |  |  |
| Volume Left | 75 | 0 | 0 | 79 | 0 |  |  |
| Volume Right | 0 | 47 | 103 | 0 | 0 |  |  |
| cSH | 384 | 742 | 1700 | 1209 | 1700 |  |  |
| Volume to Capacity | 0.19 | 0.06 | 0.21 | 0.07 | 0.14 |  |  |
| Queue Length 95th (ft) | 18 | 5 | 0 | 5 | 0 |  |  |
| Control Delay (s) | 16.6 | 10.2 | 0.0 | 8.2 | 0.0 |  |  |
| Lane LOS | C | B |  | A |  |  |  |
| Approach Delay (s) | 14.1 |  | 0.0 | 2.1 |  |  |  |
| Approach LOS B |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 3.0 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 34.3\% | ICU Level of Service |  |  | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |

Note that volumes are estimated from the base year model. HCM Unsignalized Intersection Capacity Analysis

|  | 1 |  | $\dagger$ | $p$ |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | \% | F' | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Grade | 0\% |  | 0\% |  |  | 0\% |  |
| Volume (veh/h) | 70 | 45 | 215 | 95 | 70 | 210 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.87 | 0.87 | 0.86 | 0.86 |  |
| Hourly flow rate (vph) | 77 | 49 | 247 | 109 | 81 | 244 |  |
| Pedestrians |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |
| Walking Speed (fts) |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |
| Right turn flare (veh) |  | 7 |  |  |  |  |  |
| Median type | None |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC , conflicting volume | 709 | 302 |  |  | 356 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu, unblocked vol | 709 | 302 |  |  | 356 |  |  |
| tC , single (s) | 6.4 | 6.2 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 |  |  | 2.2 |  |  |
| p0 queue free \% | 79 | 93 |  |  | 93 |  |  |
| cM capacity (veh/h) | 374 | 738 |  |  | 1202 |  |  |
| Direction, Lane \# | WB 1 | NB 1 | SB 1 | SB 2 |  |  |  |
| Volume Total | 126 | 356 | 81 | 244 |  |  |  |
| Volume Left | 77 | 0 | 81 | 0 |  |  |  |
| Volume Right | 49 | 109 | 0 | 0 |  |  |  |
| cSH | 614 | 1700 | 1202 | 1700 |  |  |  |
| Volume to Capacity | 0.21 | 0.21 | 0.07 | 0.14 |  |  |  |
| Queue Length 95th (ft) | 19 | 0 | 5 | 0 |  |  |  |
| Control Delay (s) | 14.4 | 0.0 | 8.2 | 0.0 |  |  |  |
| Lane LOS | B |  | A |  |  |  |  |
| Approach Delay (s) | 14.4 | 0.0 | 2.1 |  |  |  |  |
| Approach LOS B |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 3.1 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 34.9\% | ICU Level of Service |  |  | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |

Note that volumes are estimated from the base year model. HCM Unsignalized Intersection Capacity Analysis

|  | 7 |  | $\dagger$ |  |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | \% | 「 | $\hat{+}$ |  | * | $\uparrow$ |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Grade | 0\% |  | 6\% |  |  | -6\% |  |
| Volume (veh/h) | 80 | 85 | 255 | 95 | 90 | 250 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.87 | 0.87 | 0.86 | 0.86 |  |
| Hourly flow rate (vph) | 88 | 93 | 293 | 109 | 105 | 291 |  |
| Pedestrians |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |
| Right turn flare (veh) |  | 7 |  |  |  |  |  |
| Median type | None |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC, conflicting volume | 848 | 348 |  |  | 402 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu, unblocked vol | 848 | 348 |  |  | 402 |  |  |
| tC, single (s) | 6.4 | 6.2 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 |  |  | 2.2 |  |  |
| p0 queue free \% | 71 | 87 |  |  | 91 |  |  |
| cM capacity (veh/h) | 302 | 695 |  |  | 1156 |  |  |
| Direction, Lane \# | WB 1 | NB 1 | SB 1 | SB 2 |  |  |  |
| Volume Total | 181 | 402 | 105 | 291 |  |  |  |
| Volume Left | 88 | 0 | 105 | 0 |  |  |  |
| Volume Right | 93 | 109 | 0 | 0 |  |  |  |
| cSH | 623 | 1700 | 1156 | 1700 |  |  |  |
| Volume to Capacity | 0.29 | 0.24 | 0.09 | 0.17 |  |  |  |
| Queue Length 95th (ft) | 30 | 0 | 7 | 0 |  |  |  |
| Control Delay (s) | 16.2 | 0.0 | 8.4 | 0.0 |  |  |  |
| Lane LOS | C |  | A |  |  |  |  |
| Approach Delay (s) | 16.2 | 0.0 | 2.2 |  |  |  |  |
| Approach LOS | C |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 3.9 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 38.6\% | ICU Level of Service |  |  | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |

Note that volumes are estimated from the base year model. HCM Unsignalized Intersection Capacity Analysis

